

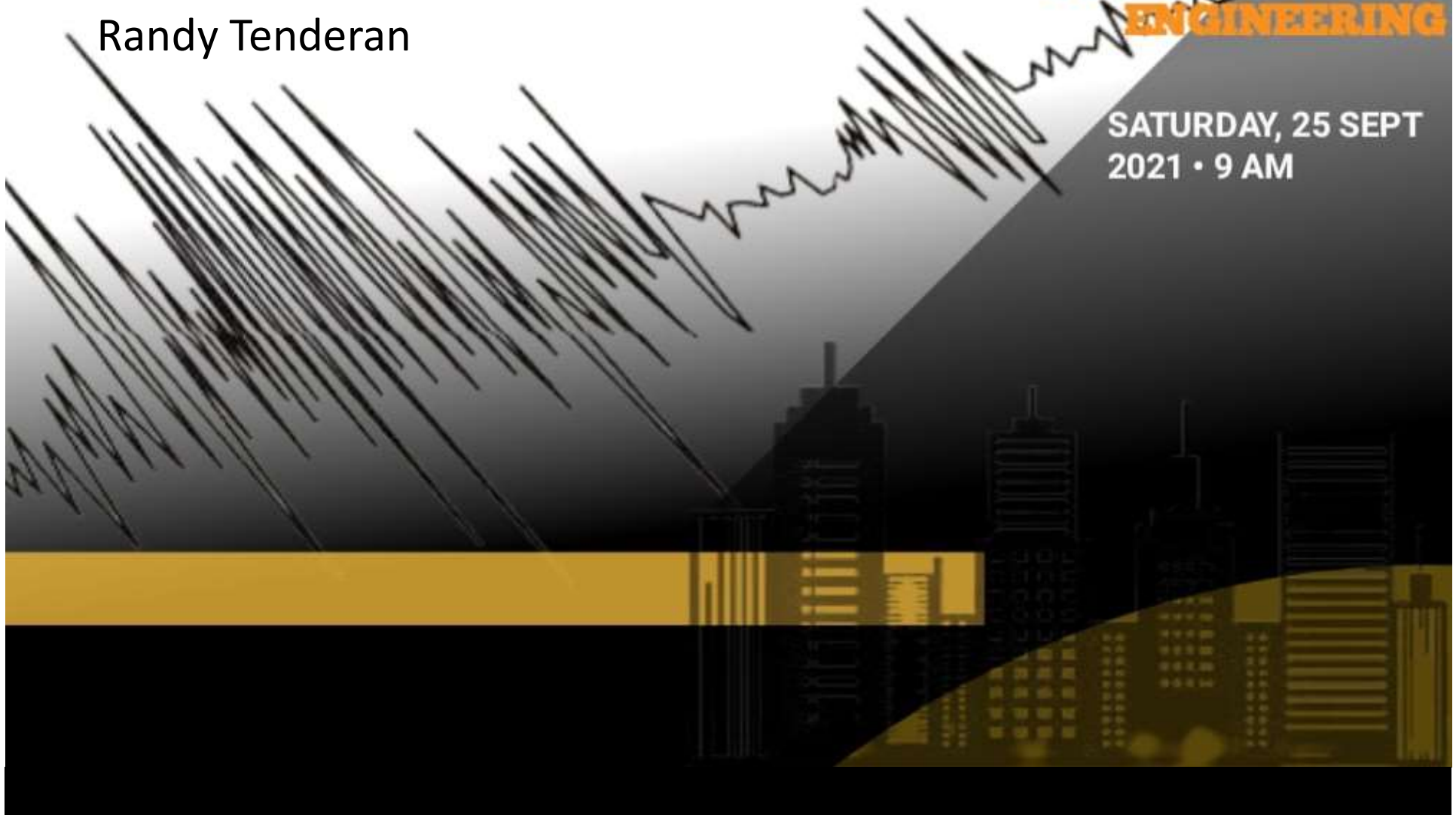
STUDY ON PERFORMANCE OF STEEL MOMENT-RESISTING FRAMES SUBJECTED TO MULTIPLE EARTHQUAKES

Randy Tenderan



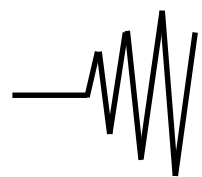
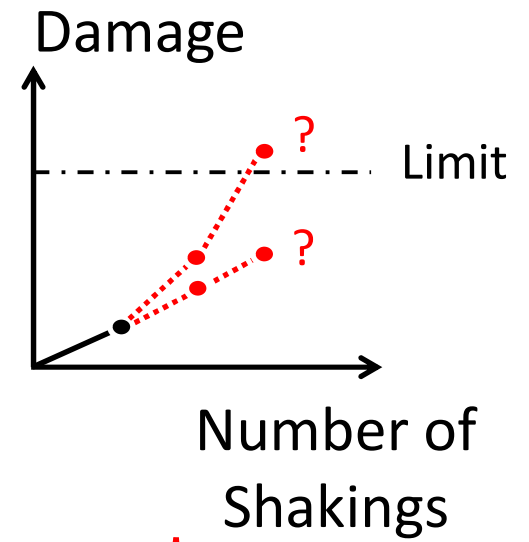
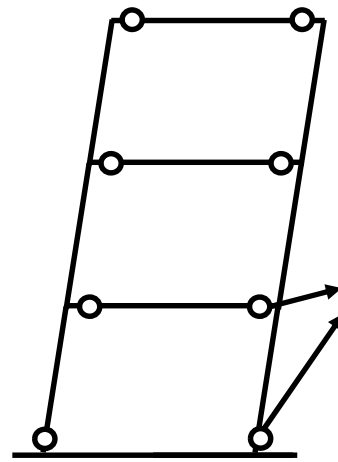
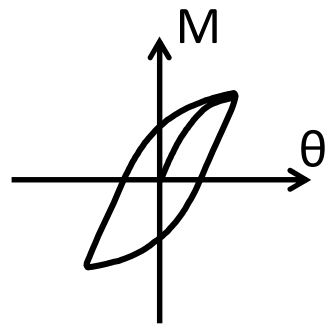
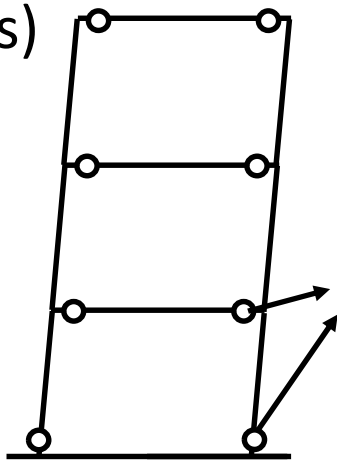
**AARGI WEBINAR
ON EARTHQUAKE
ENGINEERING**

**SATURDAY, 25 SEPT
2021 • 9 AM**

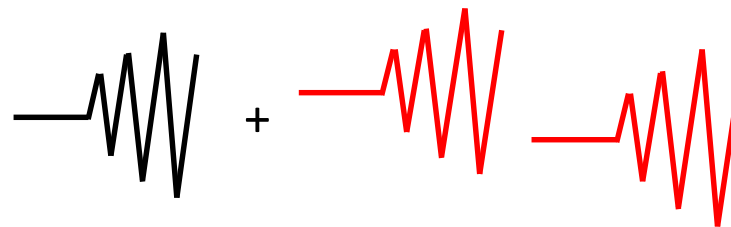


Introduction

Steel Moment Resisting Frames
(SMRFs)



Main shock



Multiple Strong Shocks



Could be guaranteed safe by following seismic design code



Seismic Performance??

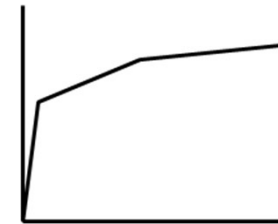
Research Objectives & Contents

Comprehensively evaluate the actual seismic performance (behavior, damage accumulation, collapse fragility) of SMRFs under multiple earthquakes

Ch. 1 Introduction

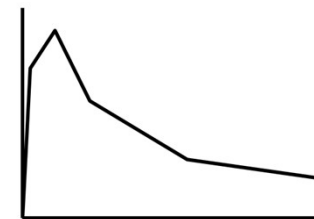
Ch. 2 Response Analysis of Nondeteriorated Models

Purpose: To evaluate the **seismic performance** of SMRFs under multiple earthquakes focusing on the **ductile fracture failure** of beam-to-column connection



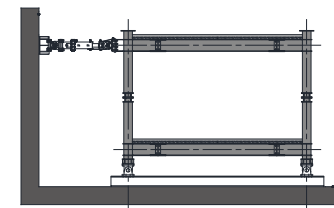
Ch. 3 Response Analysis of Deteriorated Models

Purpose: To evaluate the **seismic performance** of SMRFs under multiple earthquakes considering the **strength deterioration** caused by local buckling of columns



Ch. 4 Full-Scale Steel Frame Test

Purpose: To further verify the **seismic performance** of SMRFs under multiple earthquakes through the **experimental test**

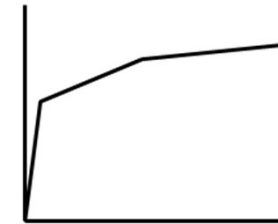


Ch. 5 Conclusions

Ch. 1 Introduction

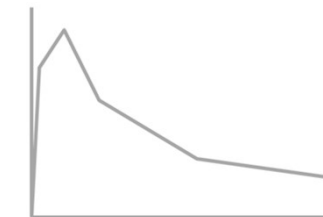
Ch. 2 Response Analysis of Nondeteriorated Models

Purpose: To evaluate the **seismic performance** of SMRFs under multiple earthquakes focusing on the **ductile fracture failure** of beam-to-column connection



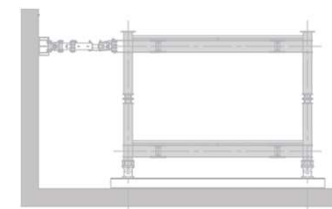
Ch. 3 Response Analysis of Deteriorated Models

Purpose: To evaluate the seismic performance of SMRFs under multiple earthquakes considering the strength deterioration caused by local buckling of columns



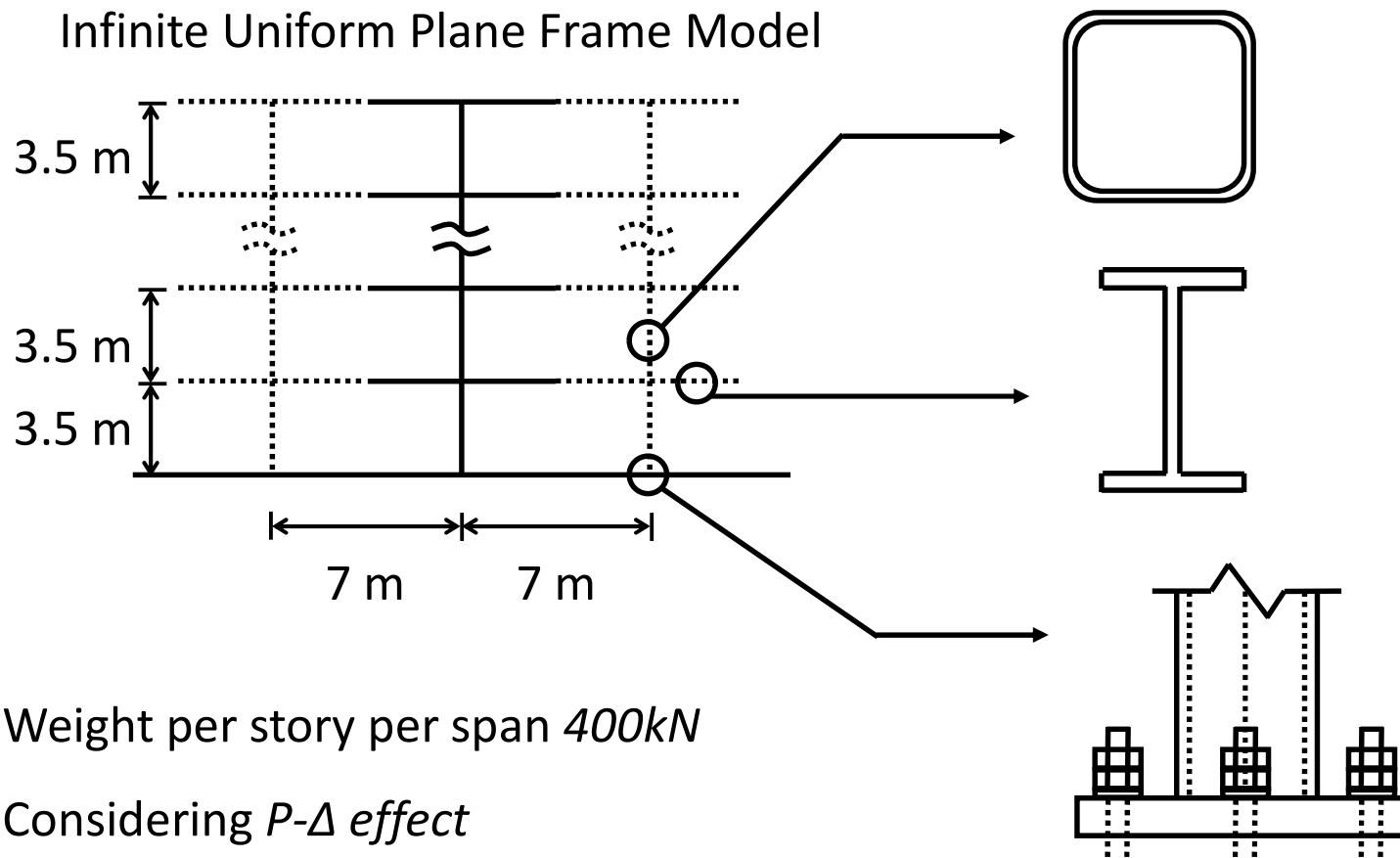
Ch. 4 Full-Scale Steel Frame Test

Purpose: To further verify the seismic performance of SMRFs under multiple earthquakes through the experimental test



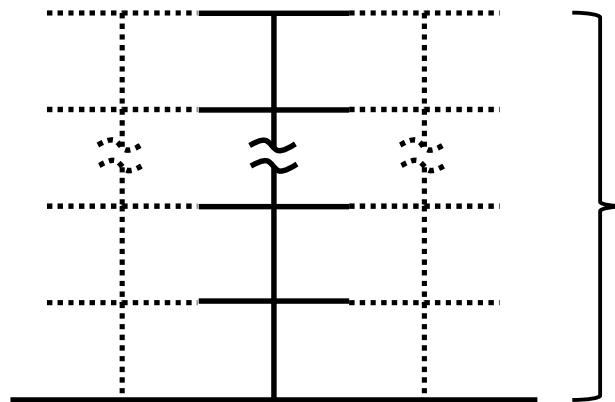
Ch. 5 Conclusions

Analytical Model



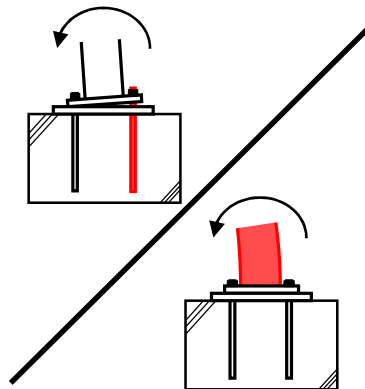
Parameter of Model

①



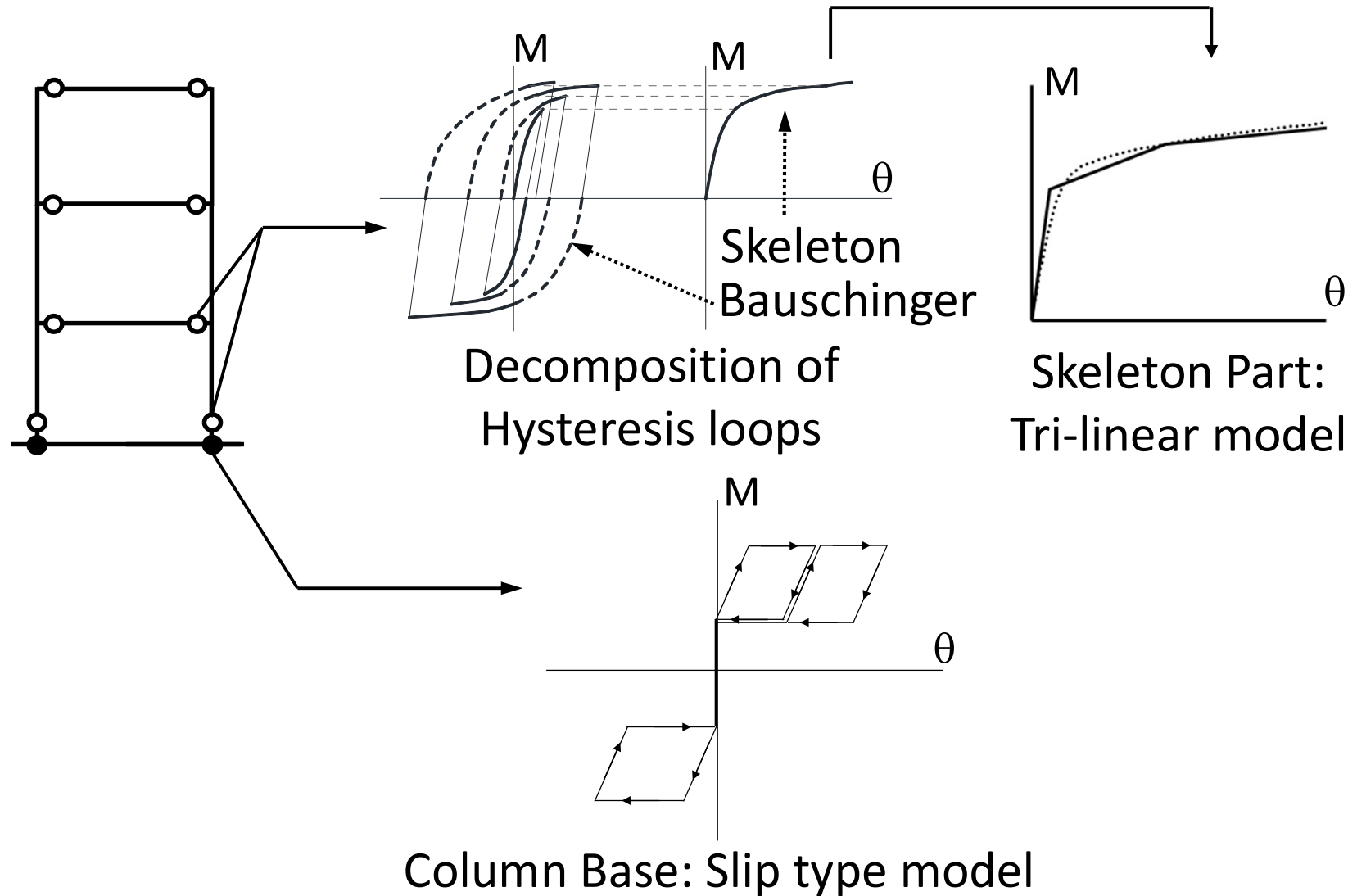
Number of Stories:
3-, 6-, and 9-story

②



$$\frac{M_{cb}}{M_{col}} = \begin{cases} 1.3 \text{ (Strong Column Base)} \\ 0.7 \text{ (Weak Column Base)} \end{cases}$$

Hysteresis Model



Input Ground Motion Records

- | | |
|-----------------------------|-----------------------------|
| 1. 1940 El Centro NS | 6. 1994 OliveView NS |
| 2. 1952 Taft EW | 7. 1995 JMA Kobe NS |
| 3. 1968 Hachinohe EW | 8. 1999 Chi Chi TCU 129 EW |
| 4. 1989 Gilroy Array #3 90° | 9. 2011 JMA Sendai NS |
| 5. 1994 Newhall NS | 10. 2016 Kik-net Mashiki EW |

Scaled to three different intensities based on Peak Ground Velocity (PGV):

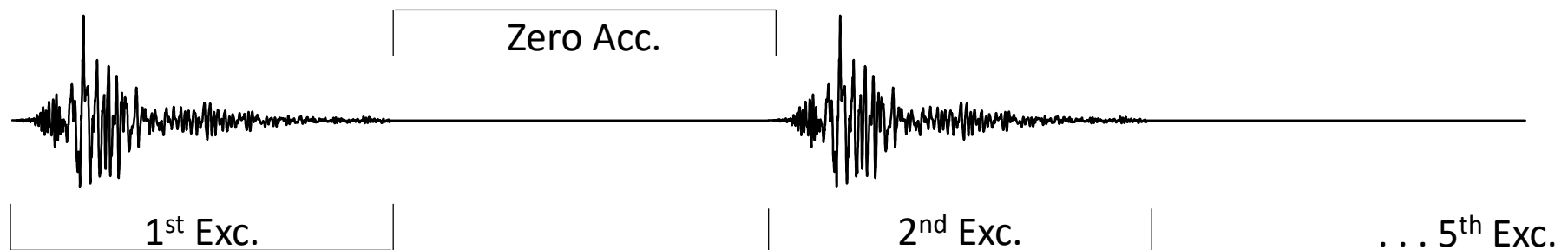
PGV 0.5 m/s (design level)

PGV 0.75 m/s

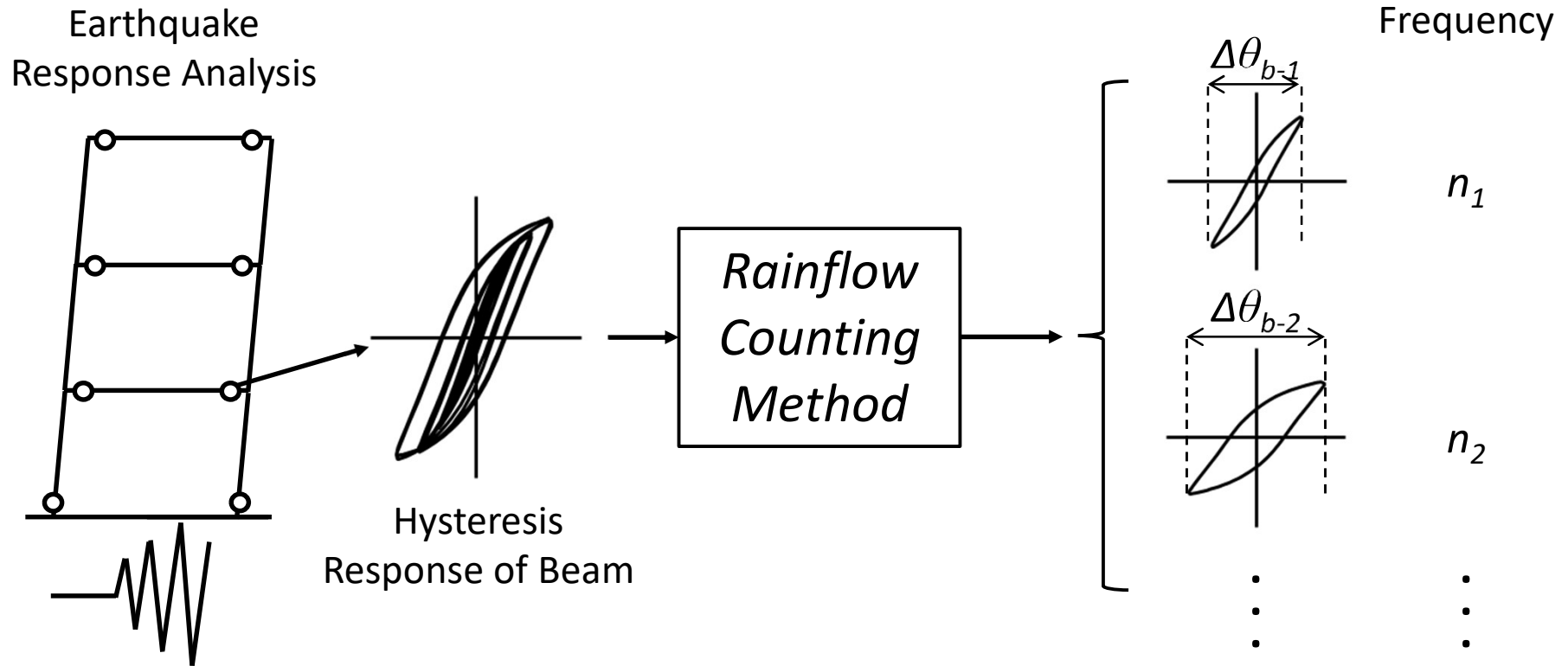
PGV 1.0 m/s

Simulation of Multiple Excitations:

Combination of 5 times excitation of Same Wave and Same Level with 30 sec. zero acceleration gap



Cumulative Damage of Beam



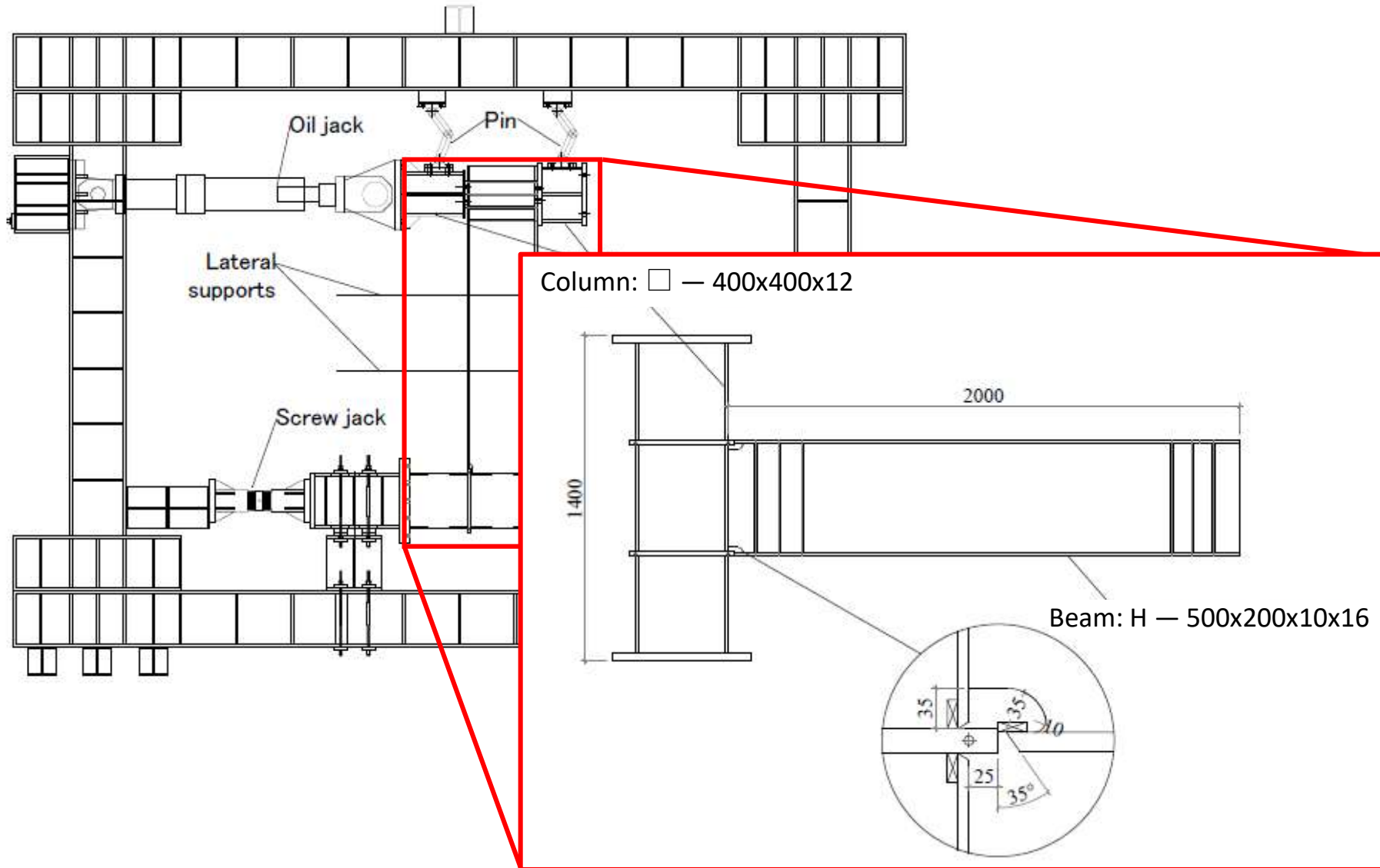
Miner's Rule: Cumulative Damage, $D = \sum_{i=1}^k \frac{n_i}{N_{fi}}$

$D \geq 1.0 \rightarrow$ Beam is estimated to be fractured

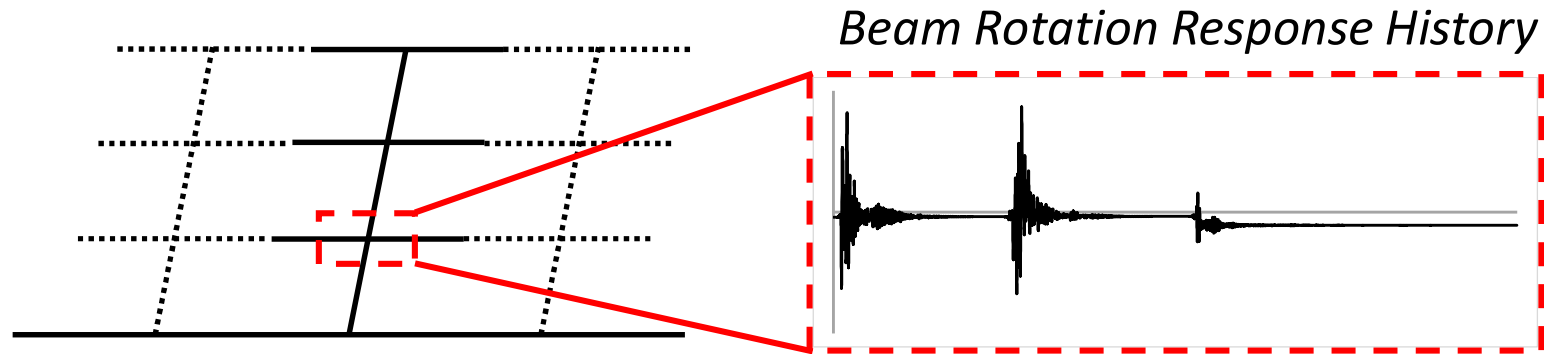
$N_f =$ The number of cycles to failure*

*Kishiki, S., Lee, D., Yamada, S., Ishida, T., and Jiao, Y., 2019. Low-Cycle Fatigue Performance Assessment of Current Japanese Steel Beam-to-Column Connections Determined by Ductile Fracture, *Engineering Structures* 182, 241–250

Outline of Test

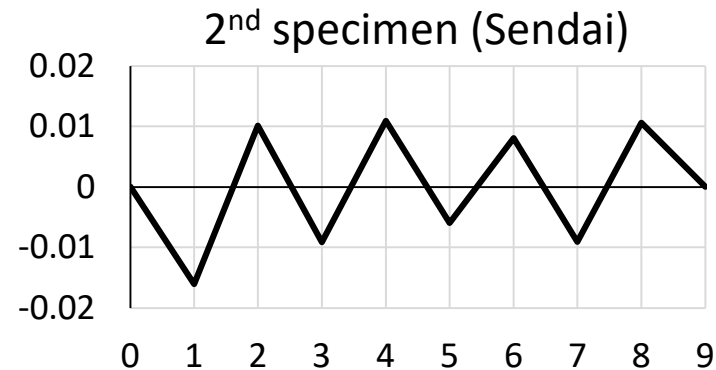
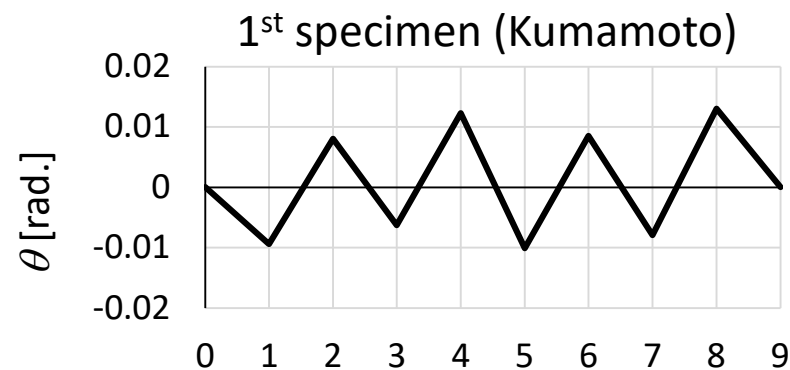


Loading History



Input Seq.	Foreshock	Main shock	Aftershock
1 st (Kumamoto)	2016/04/14-M6.5	2016/04/16-M7.3	2016/04/16-M5.9
2 nd (Sendai)		2011/03/11-M9.0	2011/04/07-M7.1

Sorted out nearly elastic cycles



Number of Sets to Fracture

1st specimen

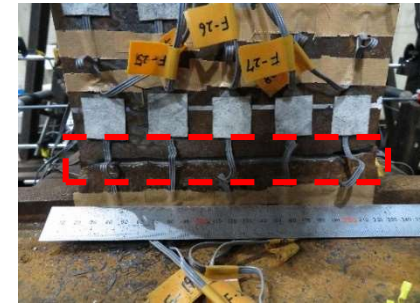
16th set: crack initiated



23rd set: crack almost penetrated through



28th set: fully fractured



$D_{calc.}$

99.1%

2nd specimen

10th set: crack initiated



17th set: crack almost penetrated through



19th set: fully fractured



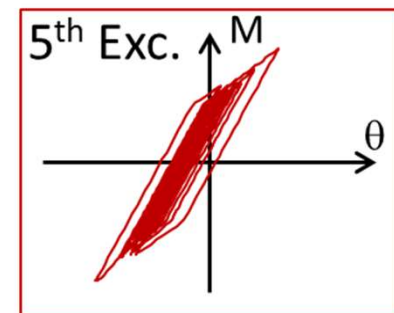
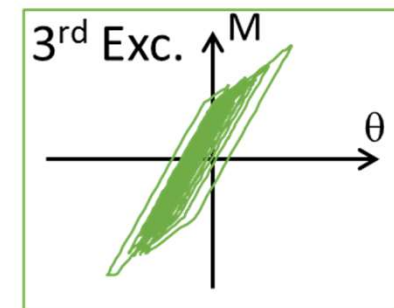
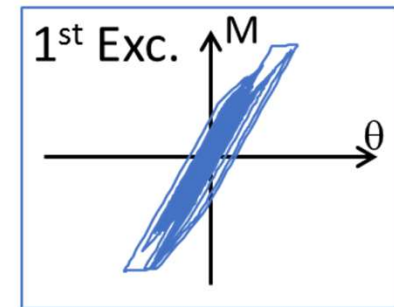
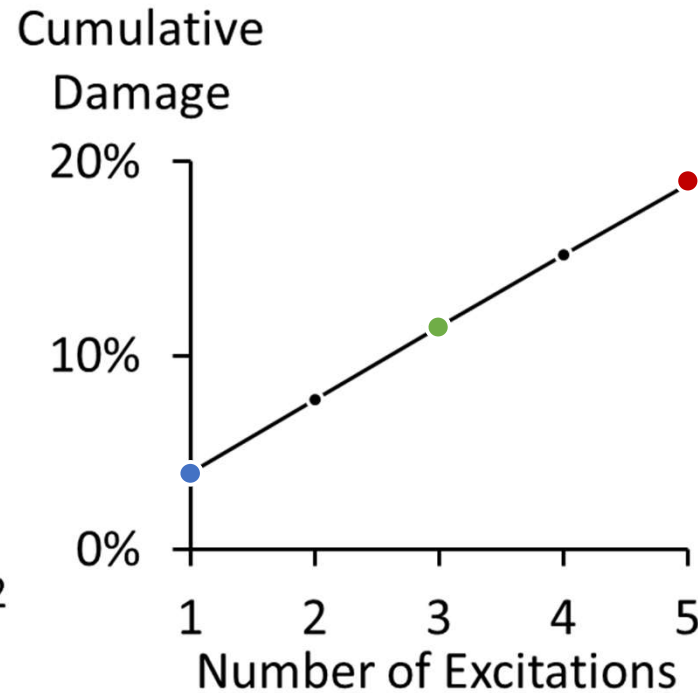
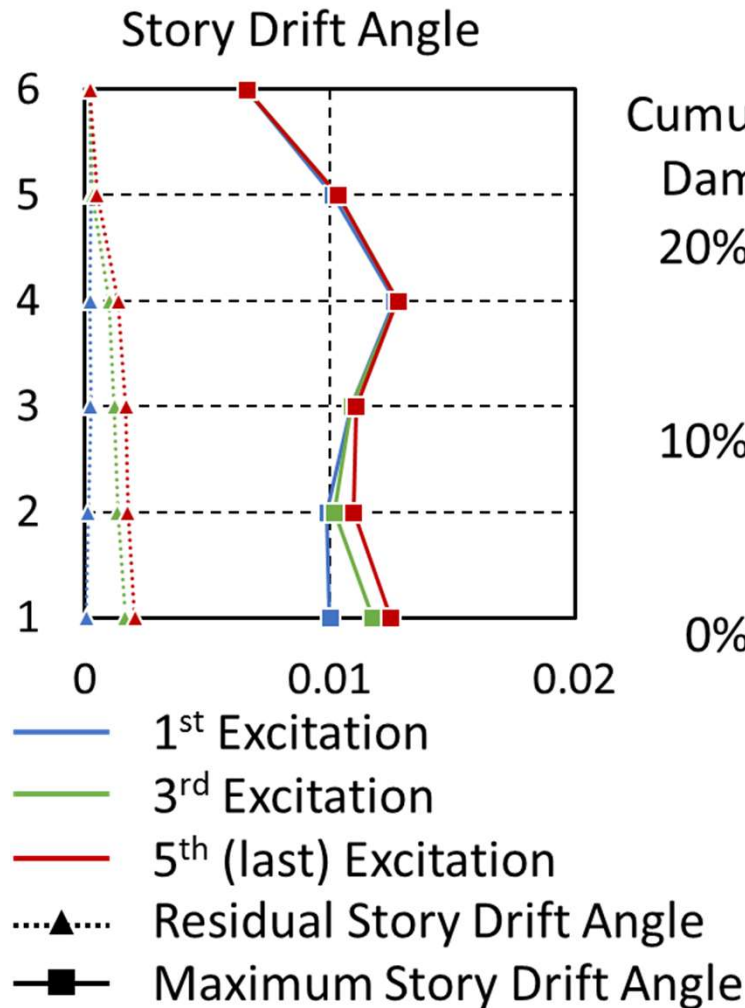
87.6%

The **reliability** of the cumulative damage evaluation method under random loading is **acceptable**

Analytical Result: PGV 0.5 m/s

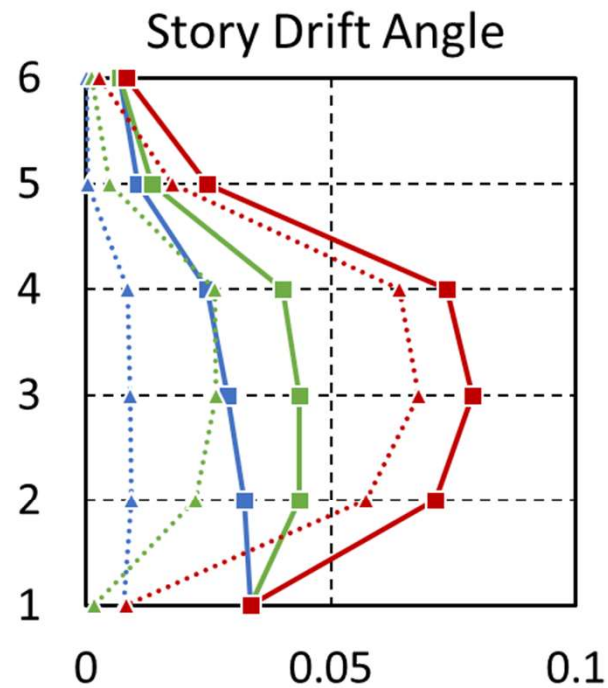
Stable Behavior

6-story Strong Col. Base Model Excited by JMA Sendai NS Record

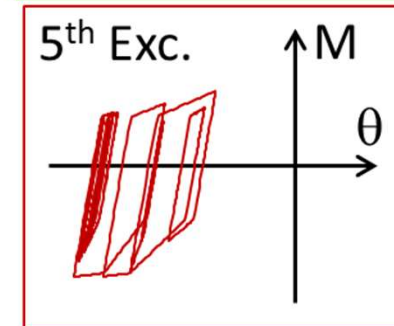
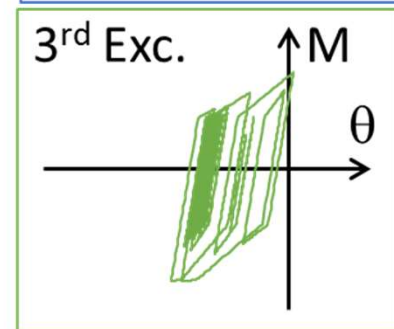
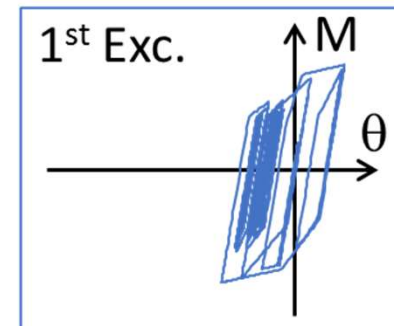
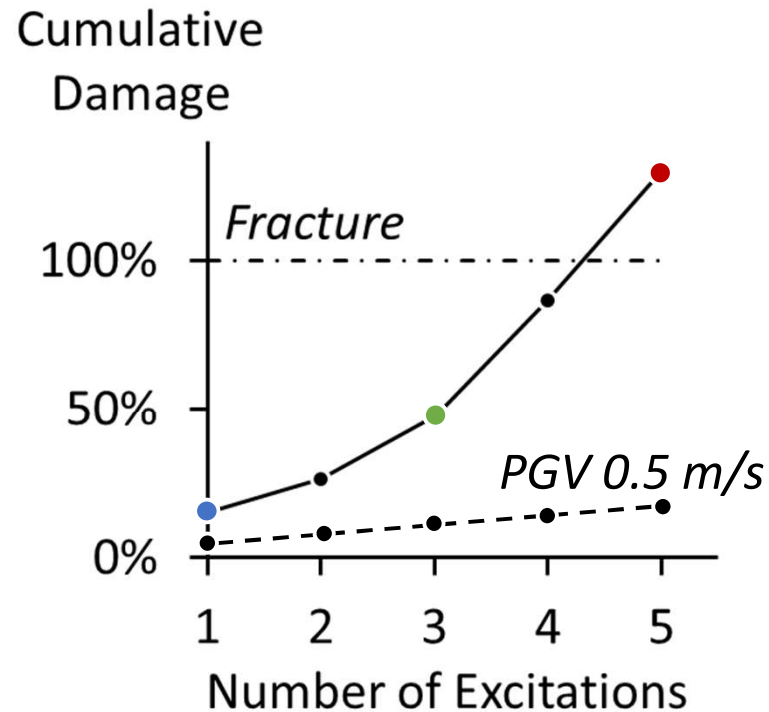


Analytical Result: PGV 0.75 & 1.0 m/s Ductile Fracture

6-story Strong Col. Base Model Excited by PGV 1.0 m/s Hachinohe EW Record

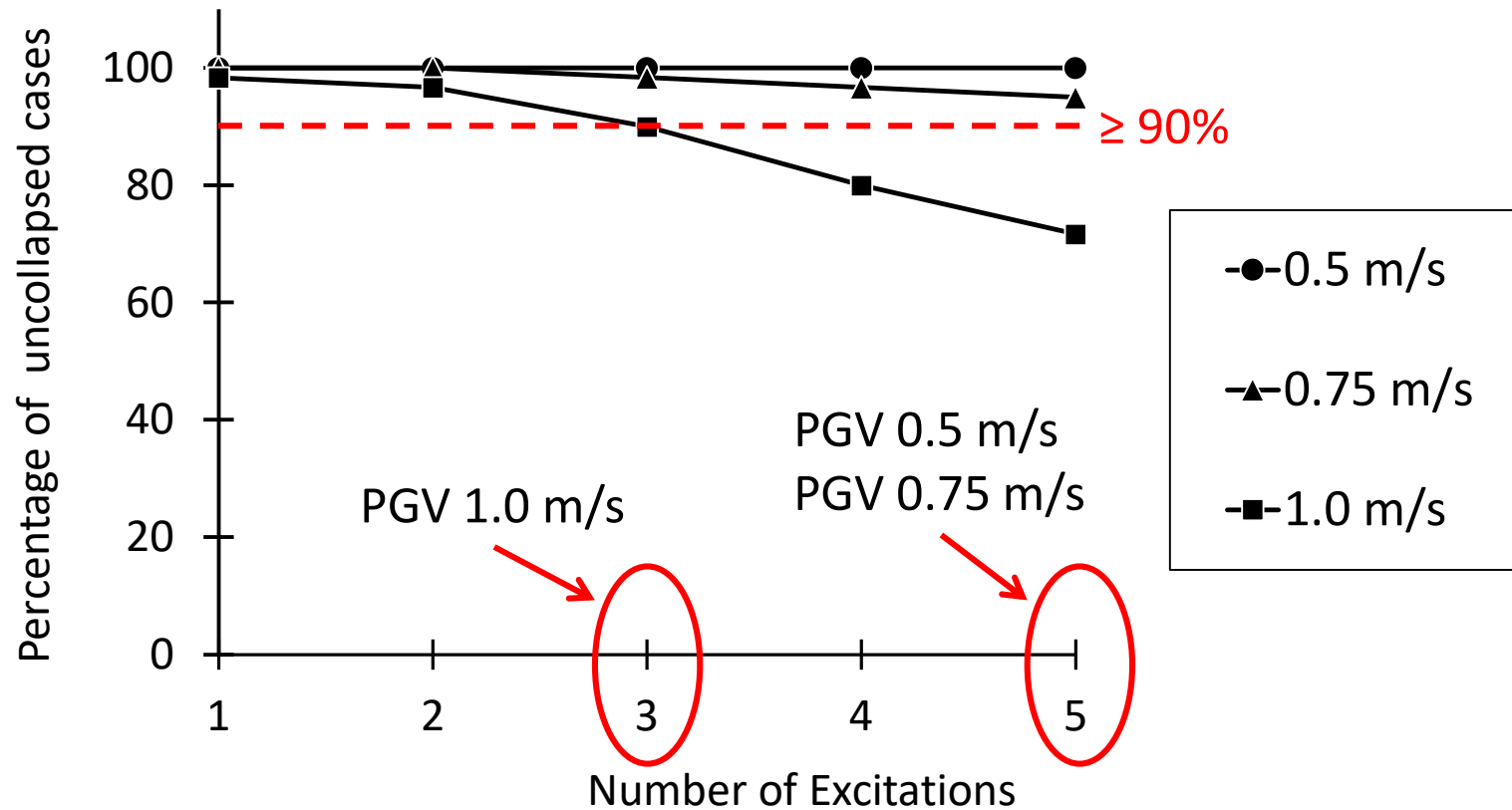


- Maximum Story Drift Angle
- ...▲... Residual Story Drift Angle
- 5th (last) Excitation
- 3rd Excitation
- 1st Excitation



Collapse Fragility

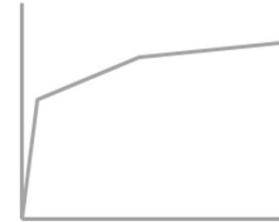
6 different models x 10 different ground motion seq. = 60 cases



Ch. 1 Introduction

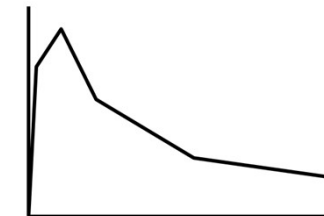
Ch. 2 Response Analysis of Nondeteriorated Models

Purpose: To evaluate the seismic performance of SMRFs under multiple earthquakes focusing on the ductile fracture failure of beam-to-column connection



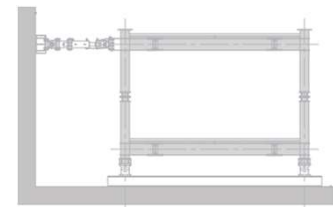
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Purpose: To evaluate the **seismic performance** of SMRFs under multiple earthquakes considering the **strength deterioration** caused by local buckling of columns



Ch. 4 Full-Scale Steel Frame Test

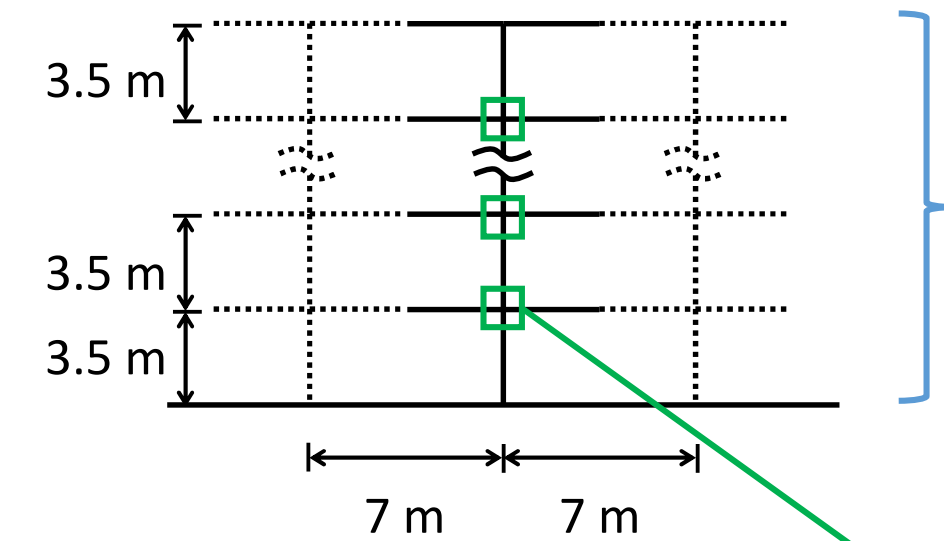
Purpose: To further verify the seismic performance of SMRFs under multiple earthquakes through the experimental test



Ch. 5 Conclusions

Parameter of Models

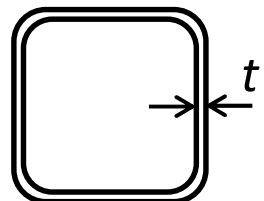
Infinite Uniform Plane Frame Model



Number of Stories:
3-, 6-, and 9-story

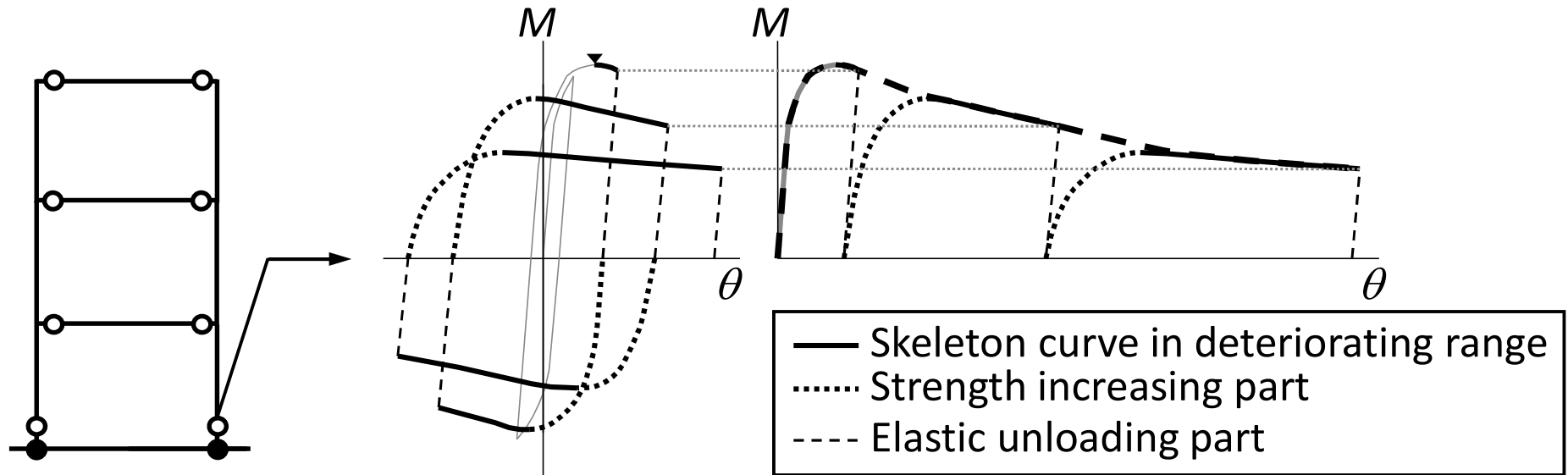
Column-to-beam moment capacity ratio ($M_p/c / M_p/b$):
1.1, 1.25, 1.5, 1.75, and 2.0

D_c
 $D_c/t = 29.45, 25, \text{ and } 20$

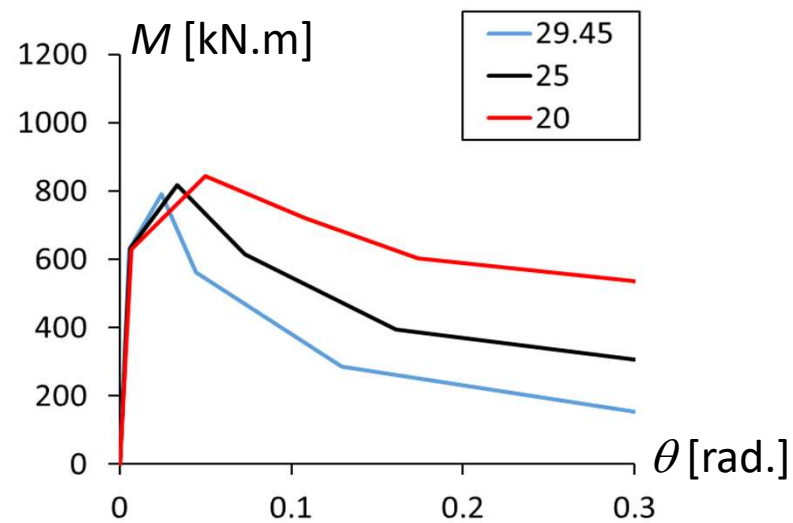


↓
Limit value for
FA rank

Hysteresis Model of Columns



Comparison of Skeleton Curve By D_c/t



Input Ground Motion Records

- | | |
|-----------------------------|-----------------------------|
| 1. 1940 El Centro NS | 6. 1994 OliveView NS |
| 2. 1952 Taft EW | 7. 1995 JMA Kobe NS |
| 3. 1968 Hachinohe EW | 8. 1999 Chi Chi TCU 129 EW |
| 4. 1989 Gilroy Array #3 90° | 9. 2011 JMA Sendai NS |
| 5. 1994 Newhall NS | 10. 2016 Kik-net Mashiki EW |

Scaled to three different intensities based on Peak Ground Velocity (PGV):

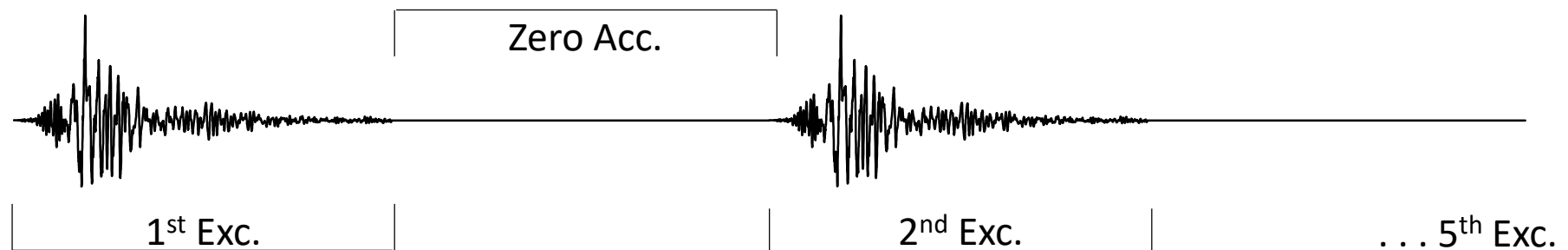
PGV 0.5 m/s (design level)

PGV 0.75 m/s

PGV 1.0 m/s

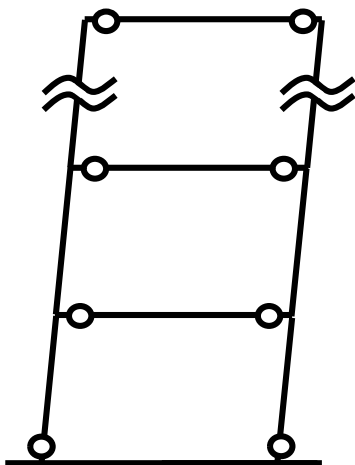
Simulation of Multiple Excitations:

Combination of 5 times excitation of Same Wave and Same Level with 30 sec. zero acceleration gap



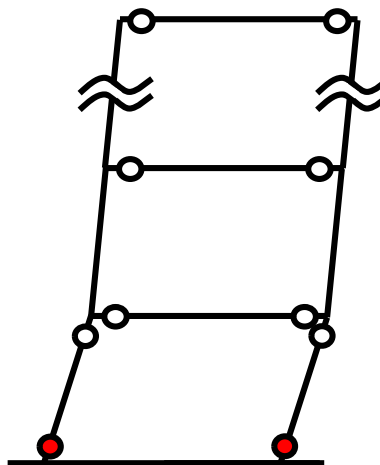
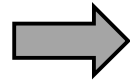
Stages to Collapse

Excitation 1 → Excitation 2 → ... → Excitation N



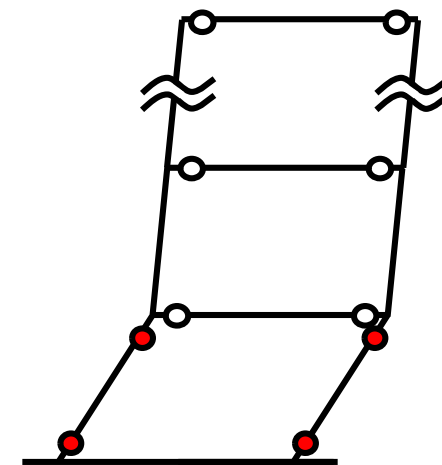
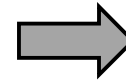
Stage 1: No deterioration

- Sway mechanism
- Stable behavior



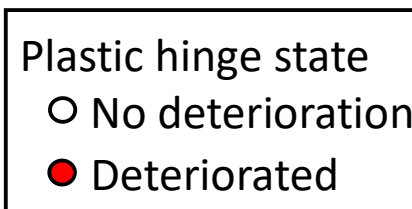
Stage 2: one end hinge of column deteriorated

- Damage concentration
- Moment redistribution



Stage 3: both end hinges of column deteriorated

- Shifting to weak story mechanism



Damage Index

Hinge condition at 1st story column

Nondeterioration Margin

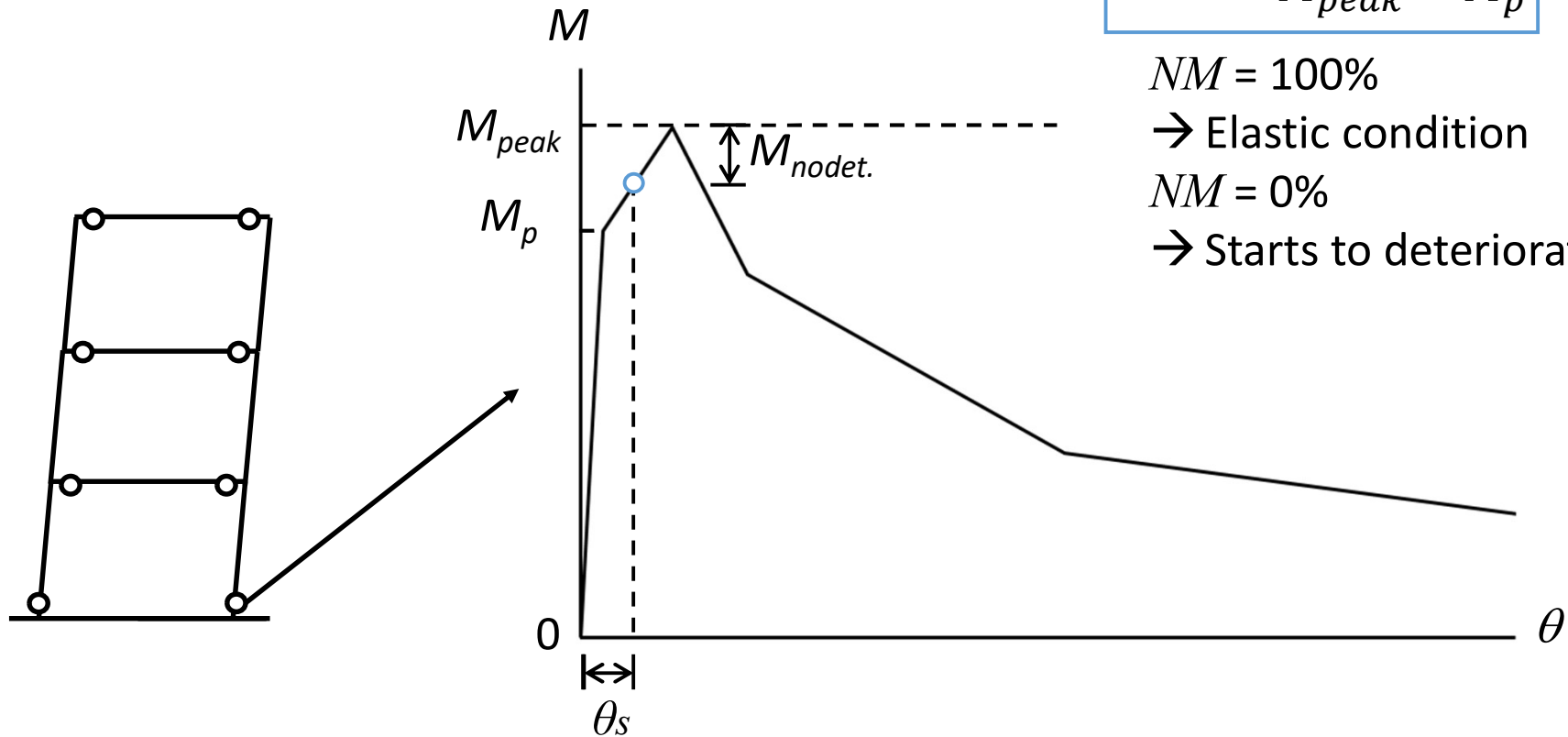
$$NM = \frac{M_{nodet.}}{M_{peak} - M_p}$$

$NM = 100\%$

→ Elastic condition

$NM = 0\%$

→ Starts to deteriorate



(Plastic Deformation
of Skeleton Part)

Damage Index

Hinge condition at 1st story column

Deterioration Index

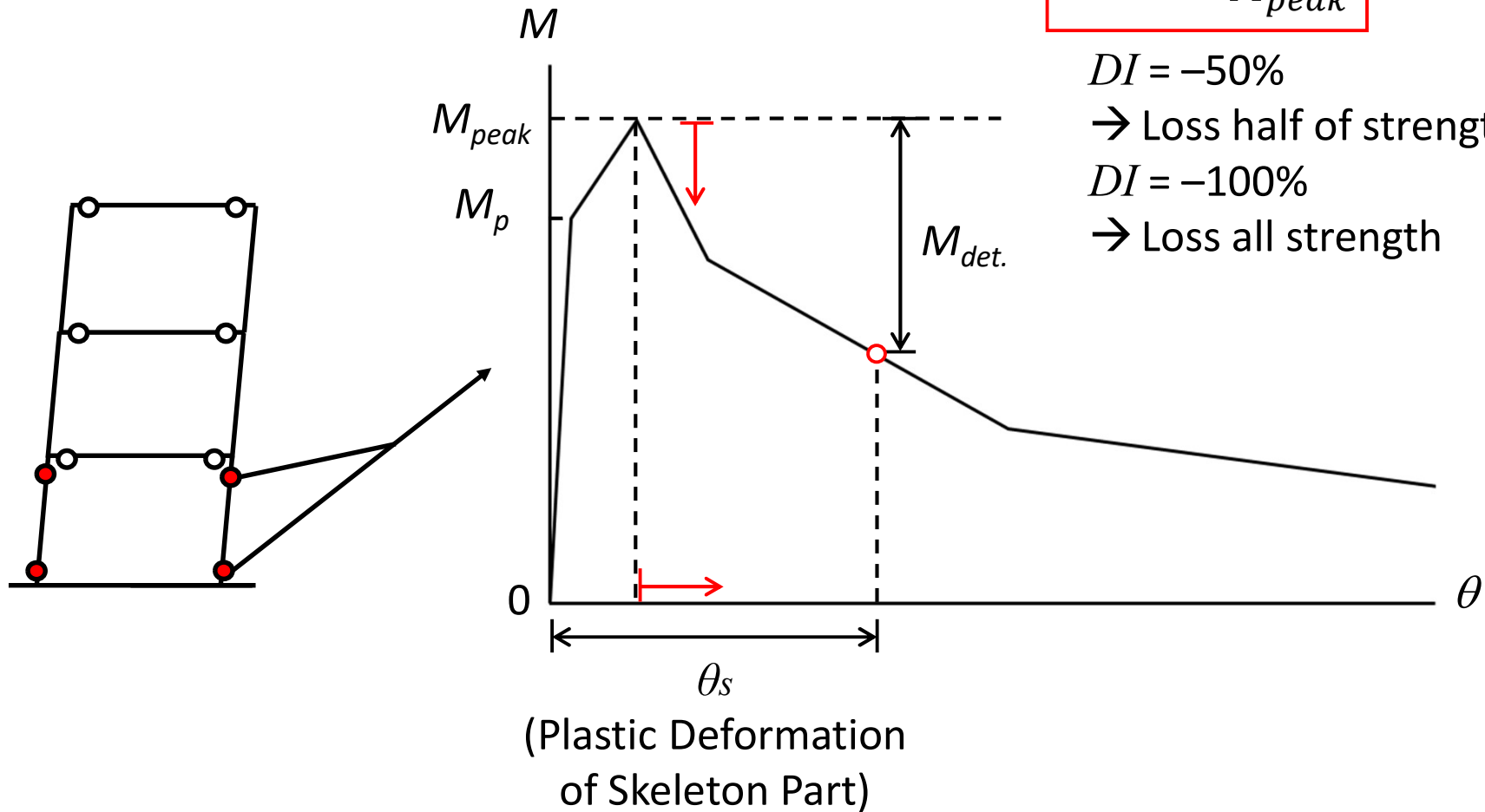
$$DI = -\frac{M_{det.}}{M_{peak}}$$

$$DI = -50\%$$

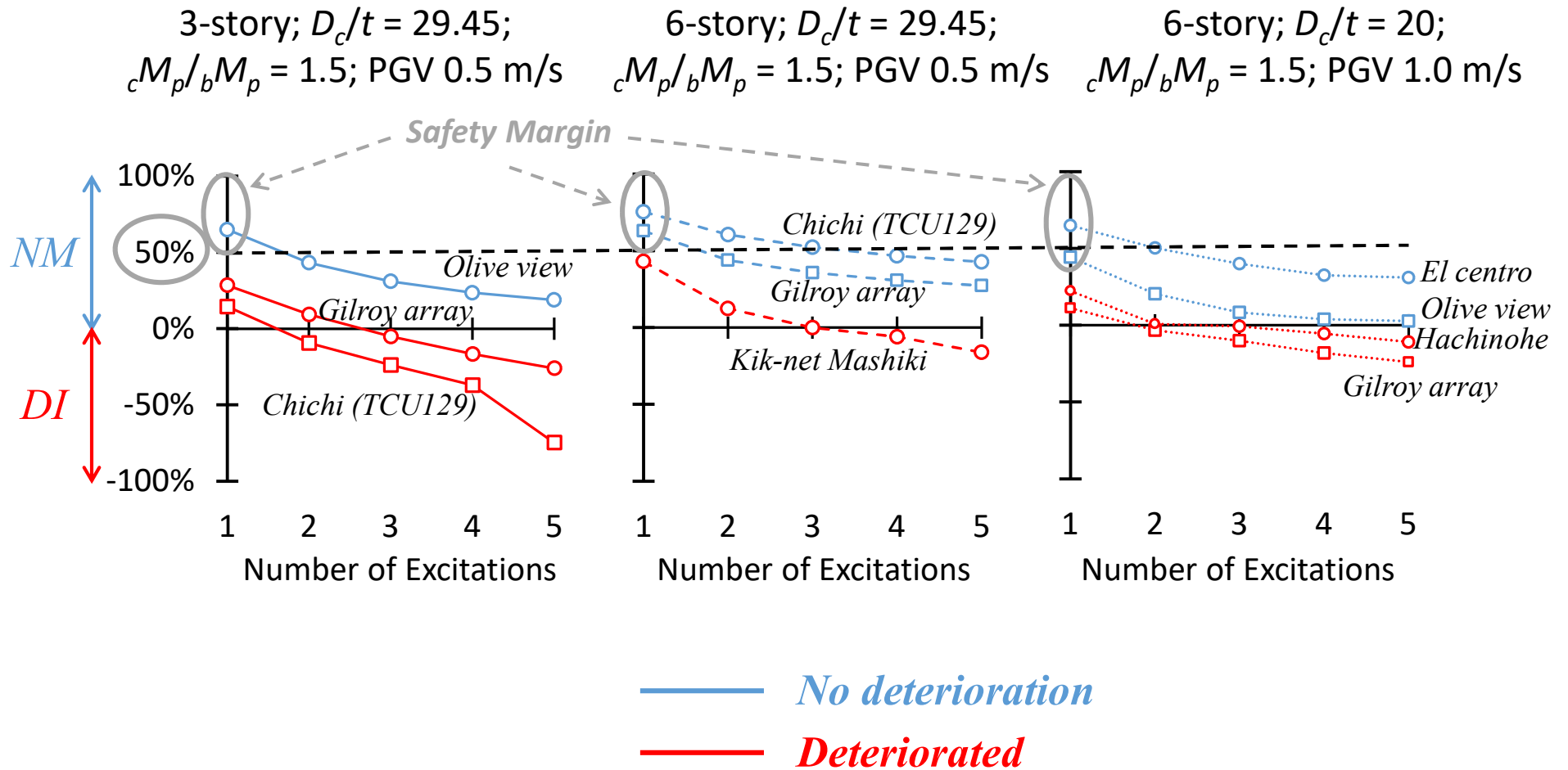
→ Loss half of strength

$$DI = -100\%$$

→ Loss all strength



Trend of Nondeterioration Margin

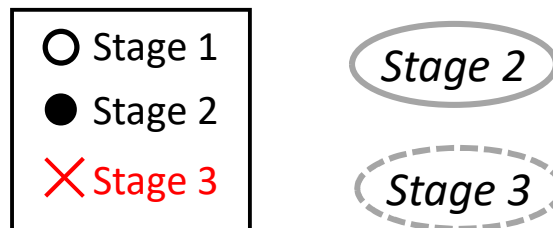
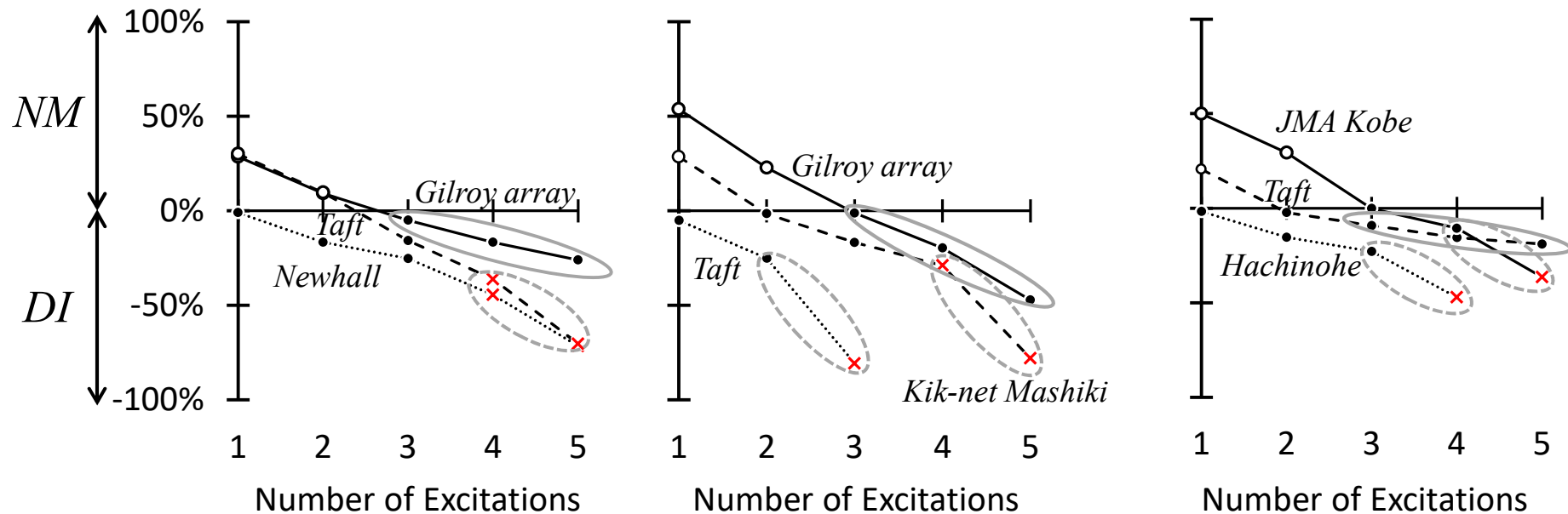


Trend of Deterioration Index

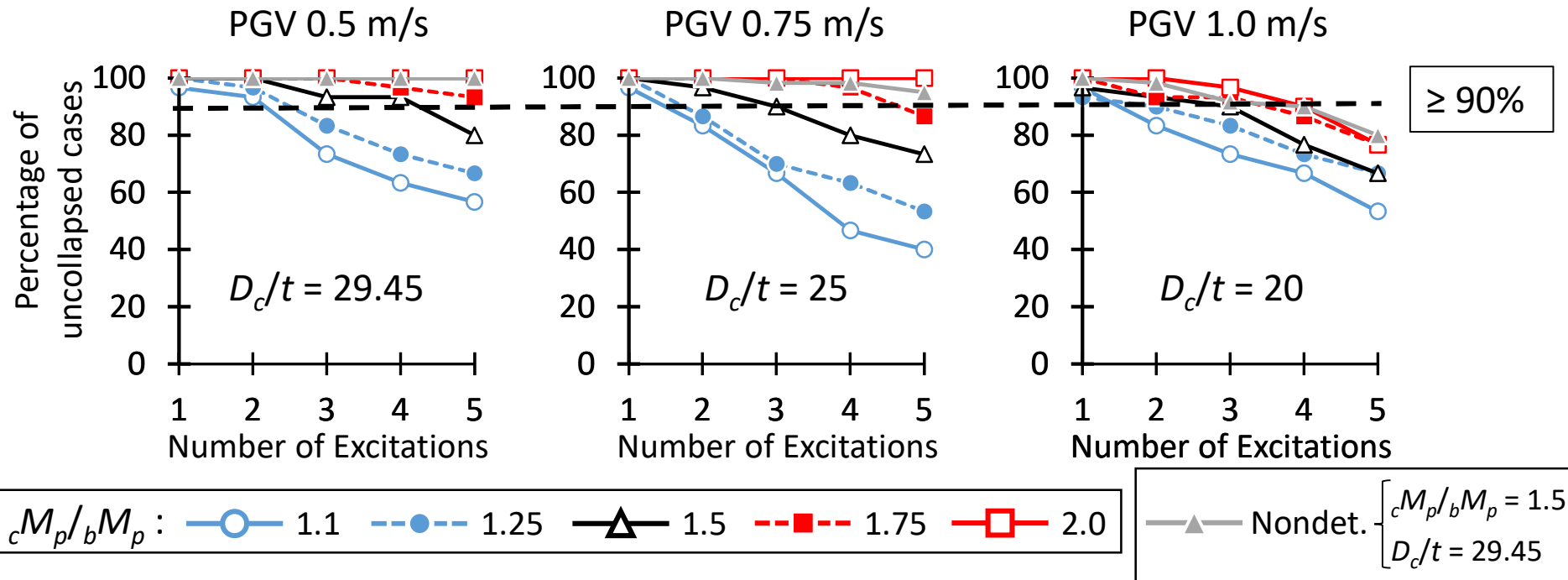
3-story; $D_c/t = 29.45$;
 $cM_p/bM_p = 1.5$; PGV 0.5 m/s

6-story; $D_c/t = 29.45$;
 $cM_p/bM_p = 1.5$; PGV 0.75 m/s

3-story; $D_c/t = 20$;
 $cM_p/bM_p = 1.5$; PGV 0.75 m/s



Collapse Fragility



Intensity (PGV)	0.5 m/s				0.75 m/s				1.0 m/s			
Number of Excitations	2	3	4	5	2	3	4	5	2	3	4	5
$D_c/t = 29.45$	1.1	1.5	1.5	1.75	1.75	2	—	—	—	—	—	—
$D_c/t = 25$	1.1	1.1	1.1	1.25	1.5	1.5	1.75	2	1.75	—	—	—
$D_c/t = 20$	1.1	1.1	1.1	1.1	1.1	1.1	1.25	1.5	1.25	1.5	2	—

Ch. 1 Introduction

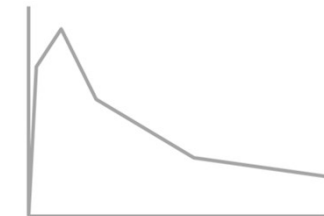
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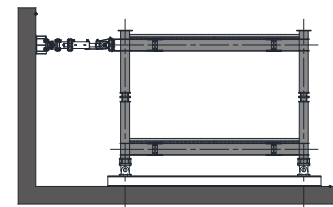
Ch. 3 Response Analysis of Deteriorated Models

Purpose: To evaluate the seismic performance of SMRFs under multiple earthquakes considering the strength deterioration caused by local buckling of columns



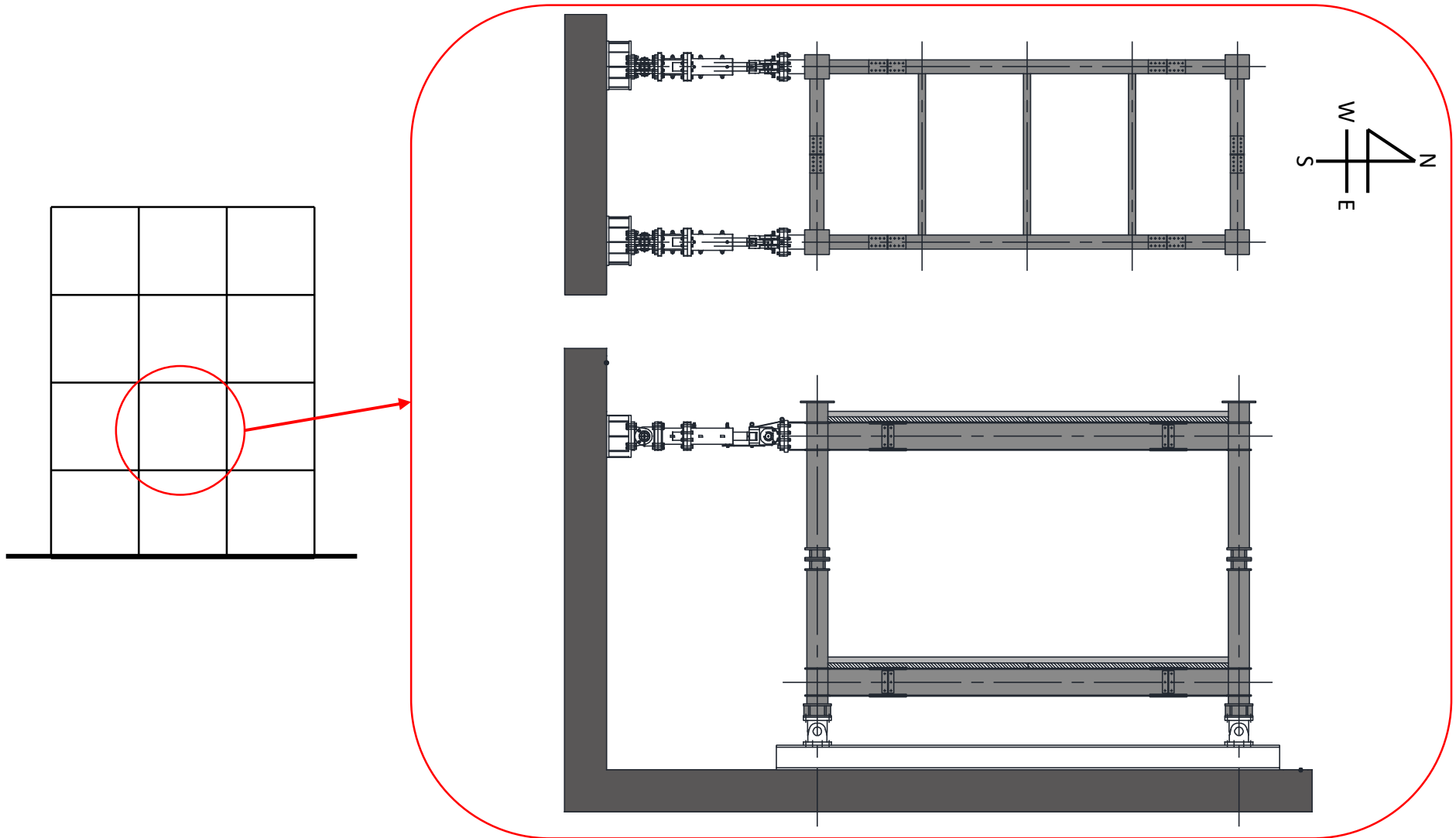
Ch. 4 Full-Scale Steel Frame Test

Purpose: To further verify the **seismic performance** of SMRFs under multiple earthquakes through the **experimental test**



Ch. 5 Conclusions

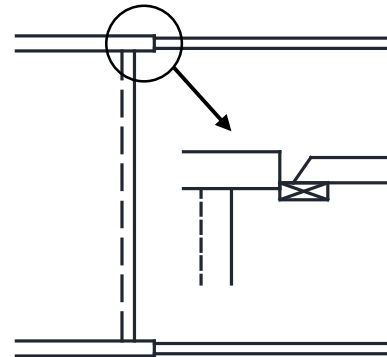
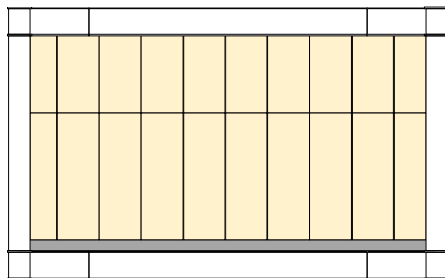
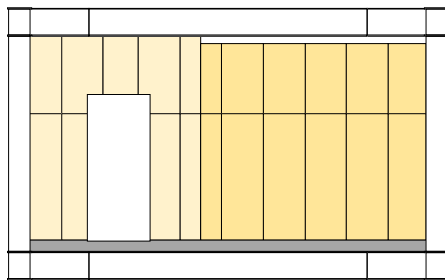
Outline of Test



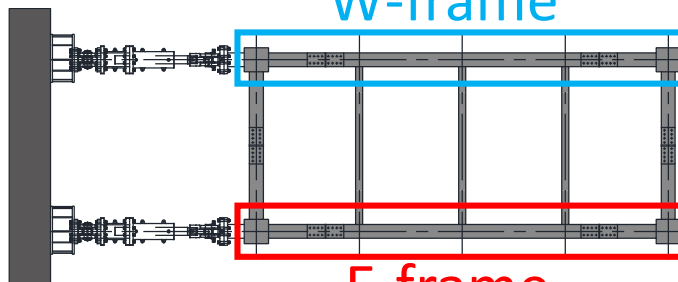
Specimens

1st specimen

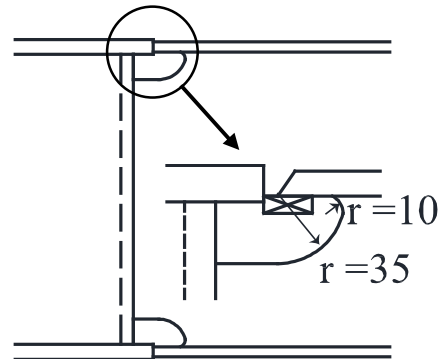
Light gauge steel
(LGS)



W-frame

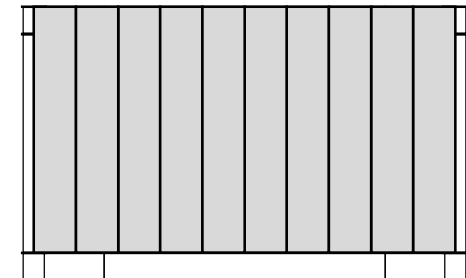
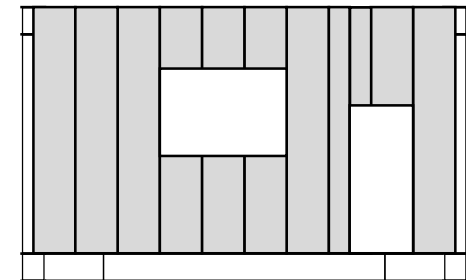


E-frame

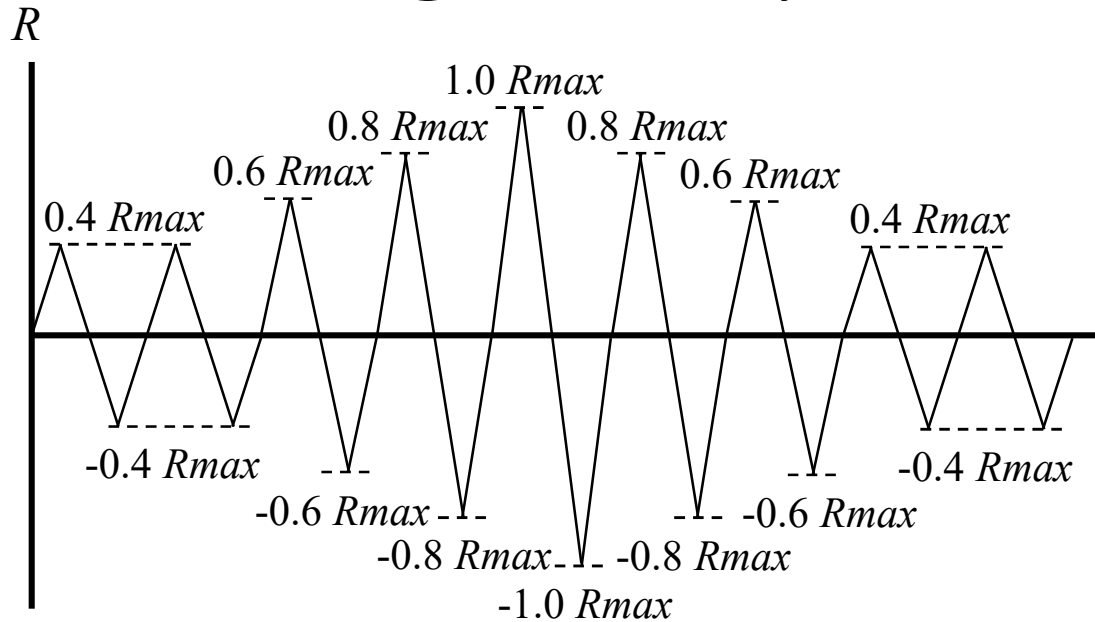


2nd specimen

Autoclaved lightweight
concrete (ALC)

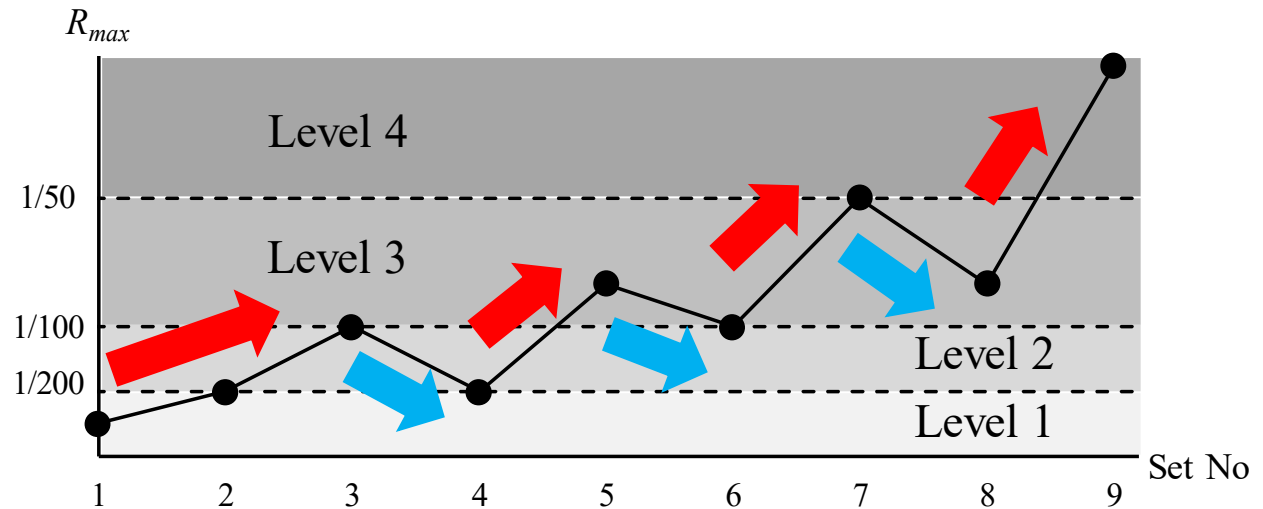


Loading History



Typical **one set** of loading represents **one earthquake**

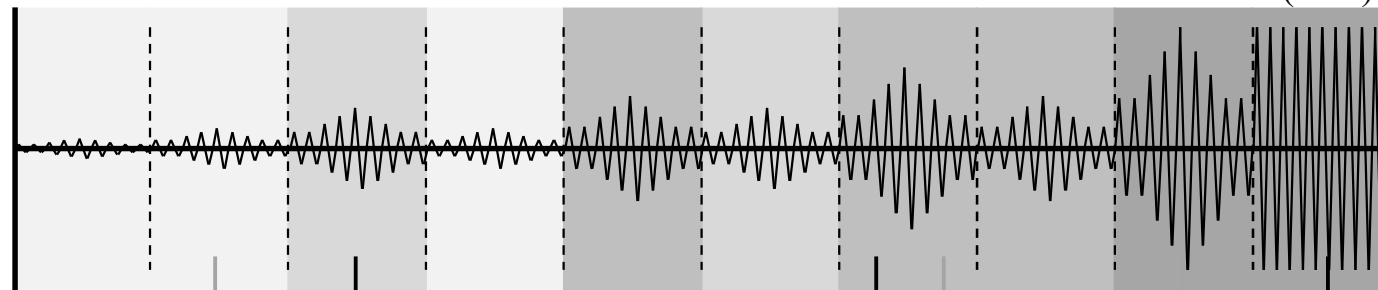
Nine sets of loading with **various levels**



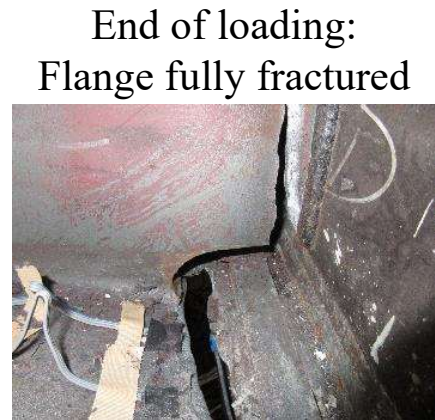
Experimental Progress

1st specimen (LGS)

Set 1	Set 2	Set 3	Set 4	Set 5	Set 6	Set 7	Set 8	Set 9	Const
1/400	1/200	1/100	1/200	1/75	1/100	1/50	1/75	1/33	(1/33)

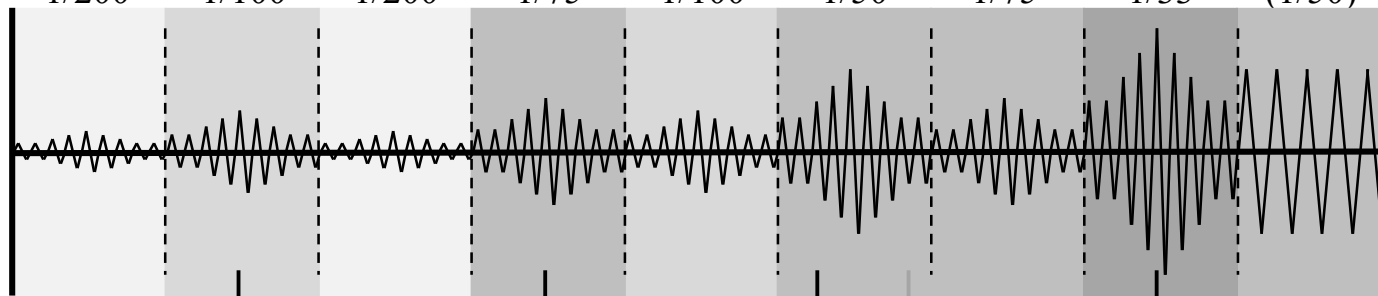


LGS board cracked | Yielded | Crack & local buckling | Board deformed out of plane | Board fell off | Crack penetrated



2nd specimen (ALC)

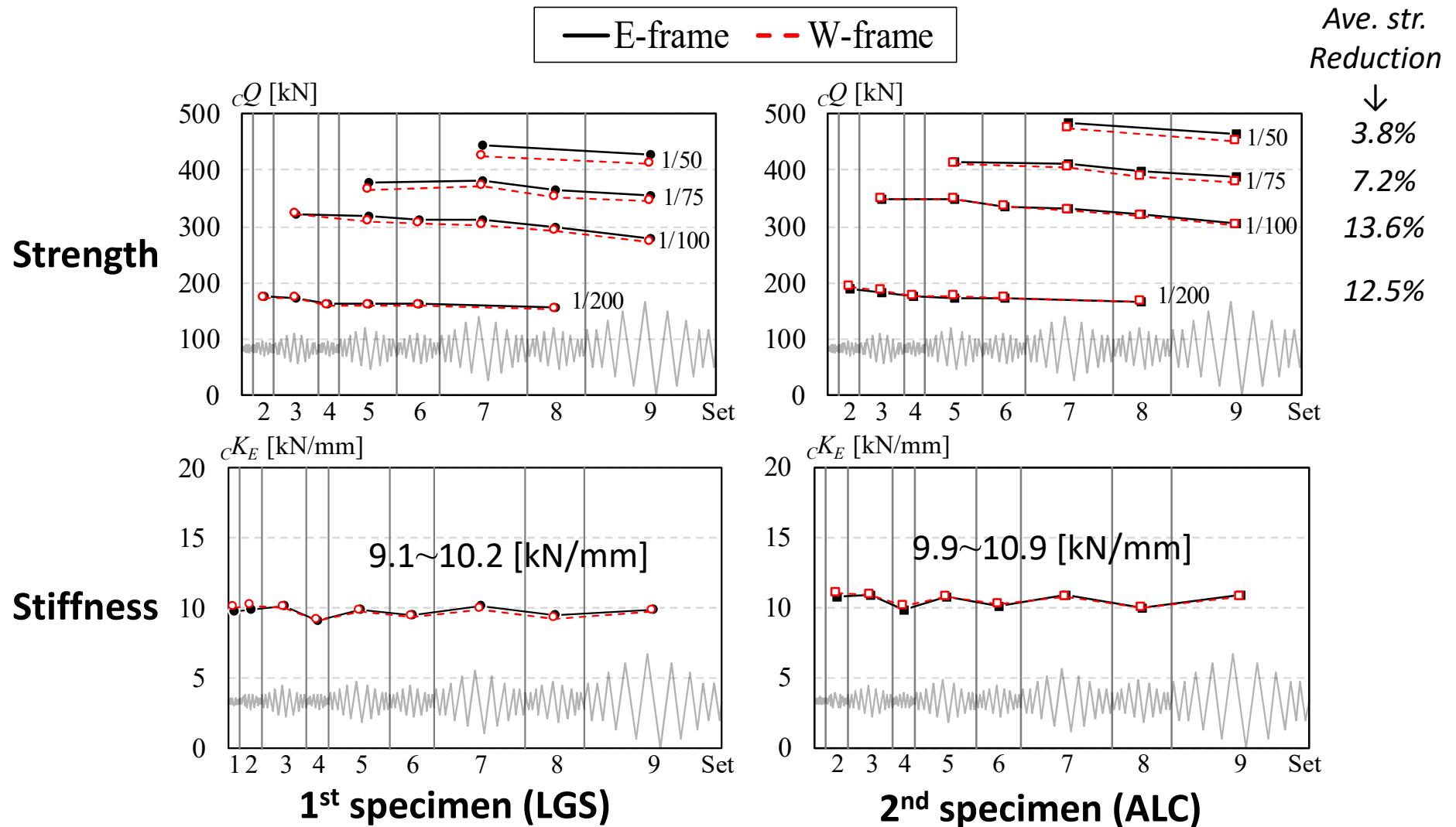
Set 2	Set 3	Set 4	Set 5	Set 6	Set 7	Set 8	Set 9	Const
1/200	1/100	1/200	1/75	1/100	1/50	1/75	1/33	(1/50)



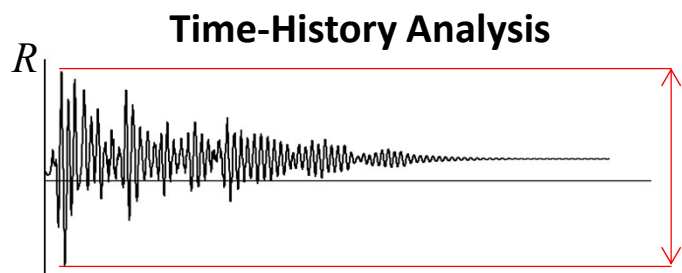
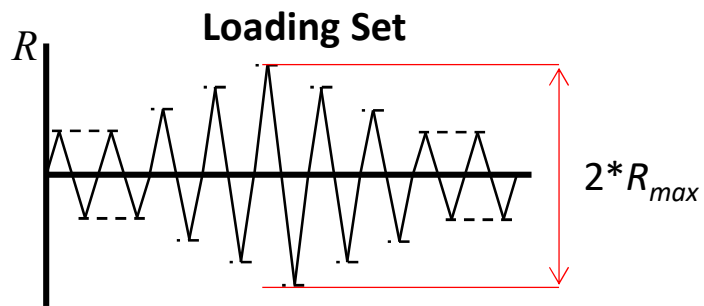
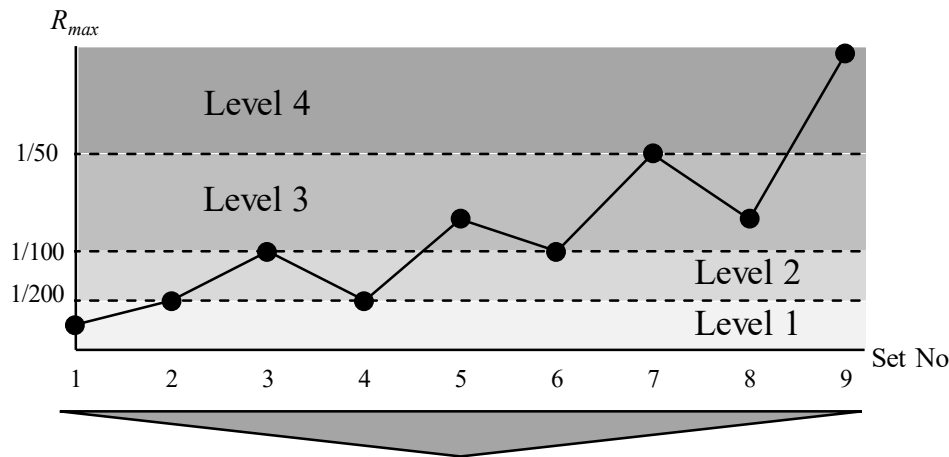
Yielded | Local buckling | Crack initiated | ALC panel cracked | Crack penetrated



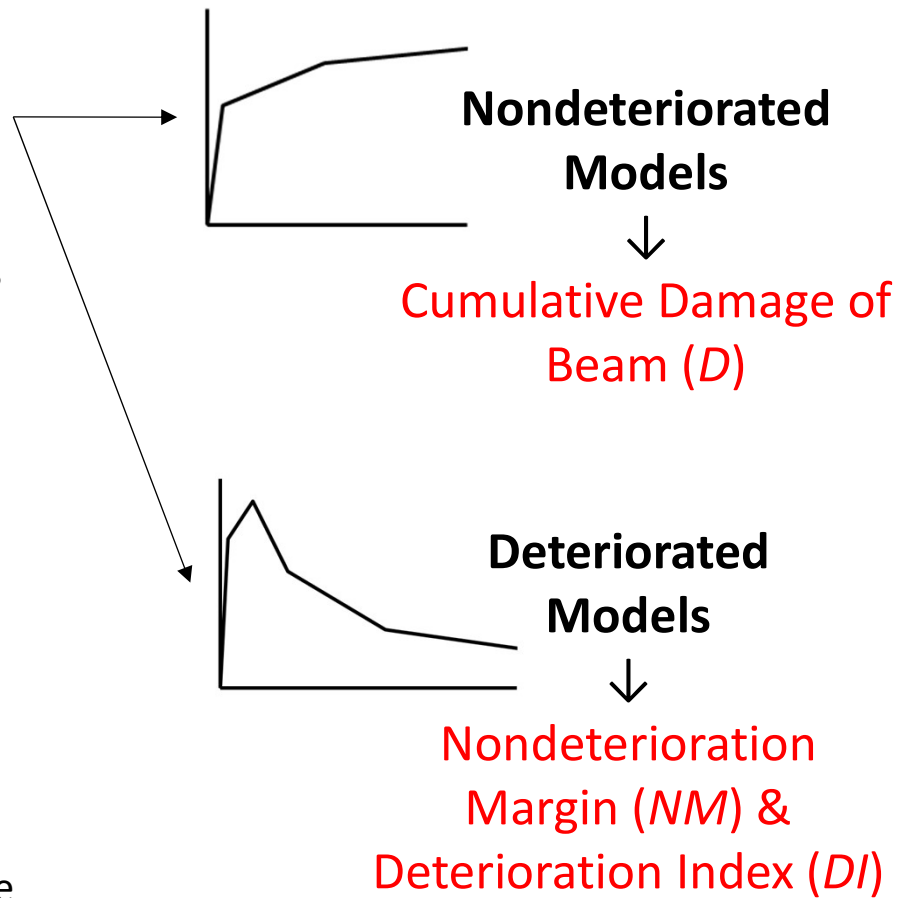
Strength and Stiffness Transition of Steel Frames



Examination by Numerical Analysis

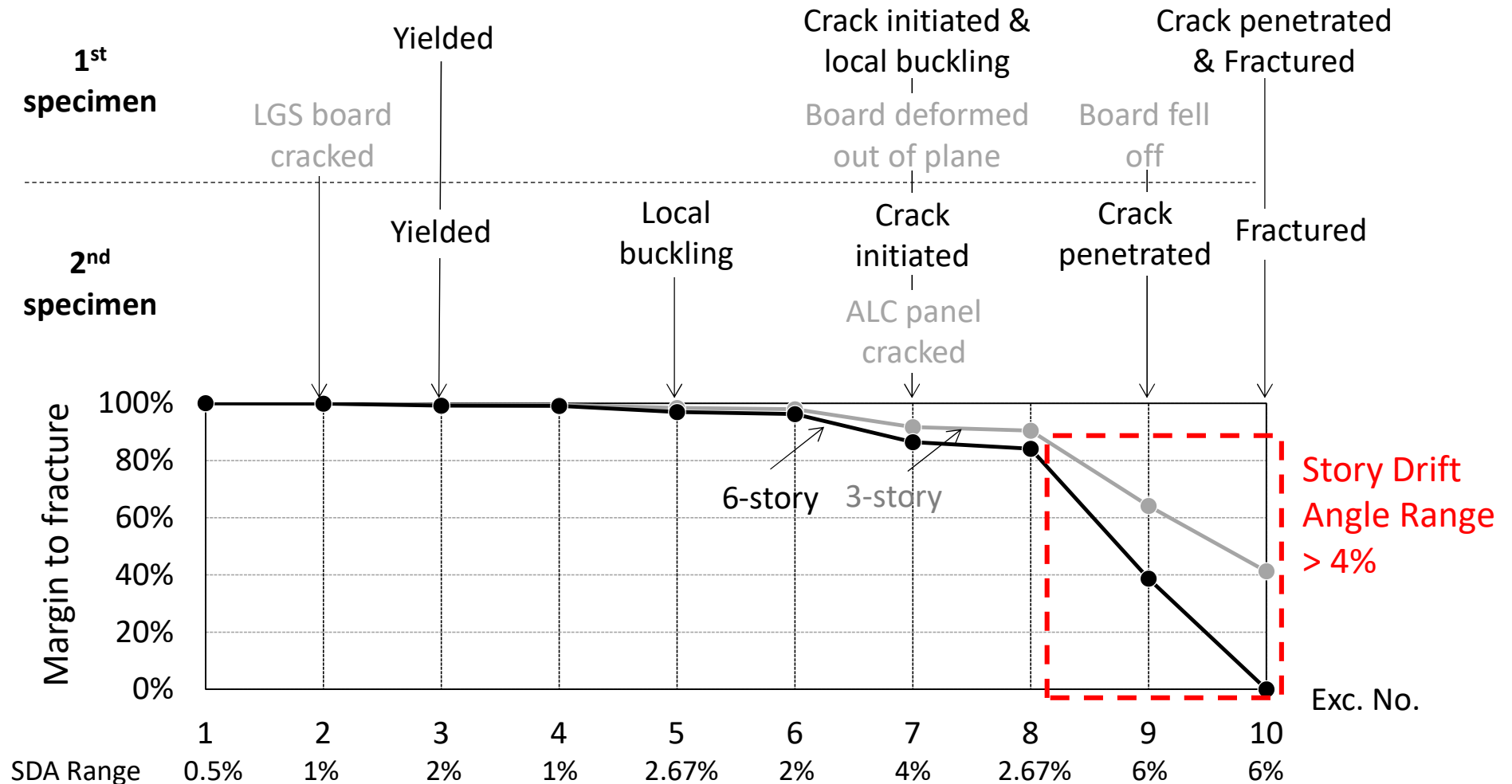


SDA Range



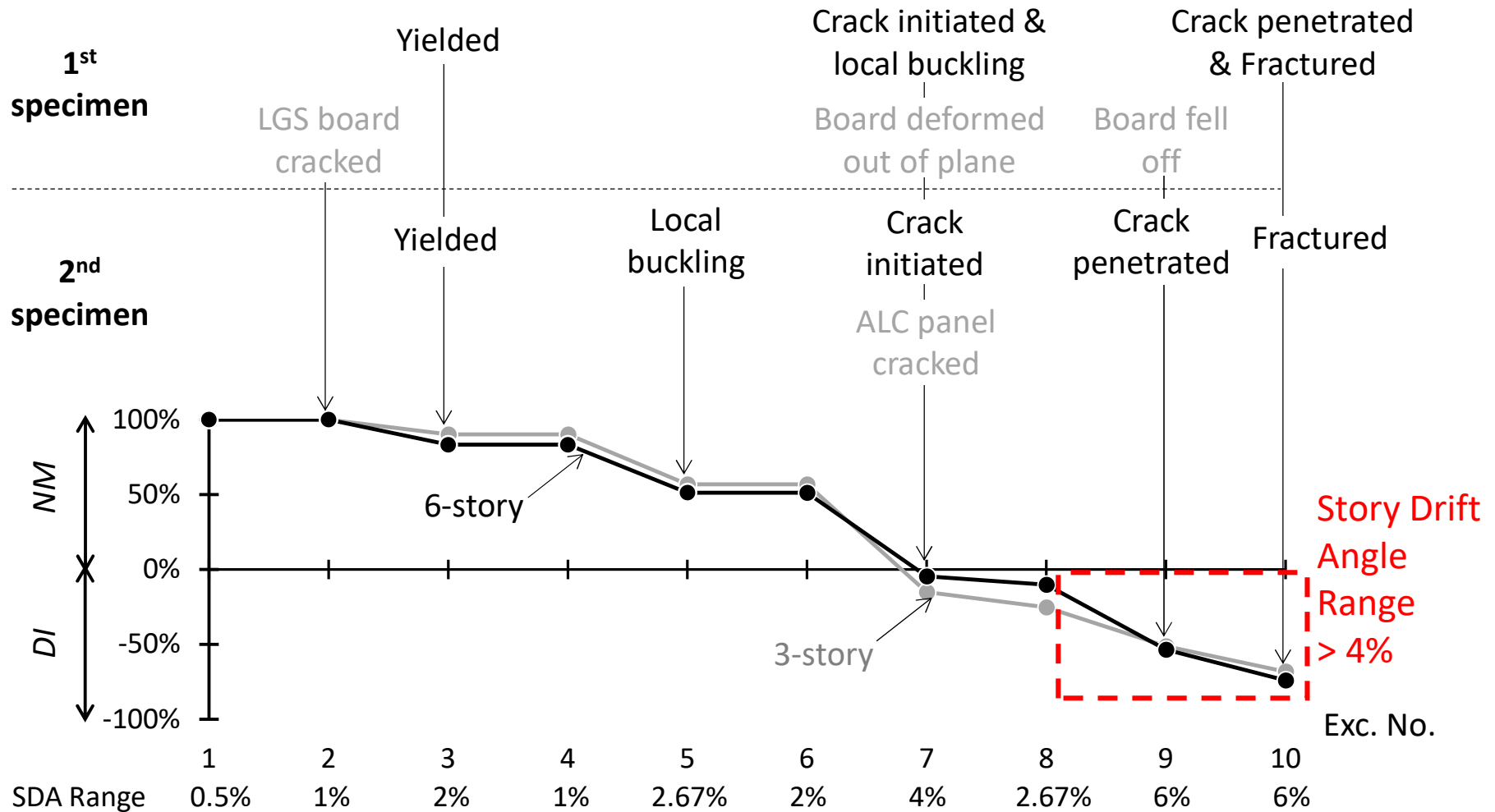
Comparison of Margin to Fracture and Observed Damages

NONDETERIORATED MODELS (Margin to fracture = 100% – cumulative damage)



Comparison of Deterioration Index and Observed Damages

DETERIORATED MODELS (*NM*: Nondeterioration margin; *DI*: Deterioration Index)



Conclusions

Ch. 2 Response Analysis of Nondeteriorated Models

- The **evaluation** is focused on the **cumulative damage at the beam end**
- Overall, the structure has a **stable behavior** and **satisfying performance**

Ch. 3 Response Analysis of Deteriorated Models

- **Story collapse** more likely to occur due to **column strength deterioration**
- Column **strength deterioration** could be **prevented** by providing enough **nondeterioration margin** at the 1st Exc.
- The **performance** could be **improved** by increasing the **column-to-beam moment ratio** or decreasing the **column width-to-thickness ratio**

Ch. 4 Full-Scale Steel Frame Test

- The **observed damages** generated within the structure and the corresponding **calculated damages** are analyzed under **various maximum story drift angle levels**
- **Severe damages** generated within the structure could be **prevented** by **limiting maximum story drift angle range** under multiple earthquakes to a certain degree

Research Papers

- **Ch. 2:** Randy Tenderan, Takanori Ishida, Yu Jiao, Satoshi Yamada. Seismic Performance of Ductile Steel Moment-Resisting Frames Subjected to Multiple Strong Ground Motions, Earthquake Spectra, Vol. 35, 1, pp. 289-310, Feb. 2019.
- **Ch. 3:** Randy Tenderan, Takanori Ishida, Satoshi Yamada. Effect of Column Strength Deterioration on the Performance of Steel Moment-Resisting Frames Subjected to Multiple Strong Ground Motions, Engineering Structure. (under review)
- **Ch. 4:** Takanori Ishida, Randy Tenderan, Keita Kohtaki, Shoichi Kishiki, Jun Iyama, Takashi Hasegawa, Tsuyoshi Seike, Satoshi Yamada. Experimental Study on Full-Scale Steel Moment-Resisting Frames Considering Multiple Earthquakes, Engineering Structure 2021.